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い非常にコンパクトな画像表示装置を提供することがで
きる。

[0.084] 本発明のもう1つの画像形成装置は、画像表示素子と、前記画像表示素子により形成された画像を
映像として観察できるように導く接眼光学系とを有する
画像表示装置において、前記接眼光学系は、少なくとも
3面で形成される空間を屈折率が1より大きい媒質で満
たしており、前記少なくとも3面は、観察者眼鏡直前に
位置している屈折及び内部反射面と、前記屈折及び内部
反射面に対向し前記接眼光学系の外周部に配置された外
界側内部反射面と、前記画像表示素子の発する光束を入
射する屈折面とかなり、その中の少なくとも1面が、
観察者視軸に対して偏心あるいは傾いた面で構成され、
少なくとも3回の内部反射をしている偏心プリズムと、
前記屈折及び内部反射面に位置している屈折及び内部反射面
と前記外界側内部反射面とを介して外界を観察する組
合、外界光に対する前記2面で発生するパワーを打ち消
す作用を有する第2光学素子とかなり、前記第2光学
素子は前記外界側内部反射面の外周側に配置されている
ことを特徴とするものである。

[0.085] 観察者眼鏡直前に位置している第1面と、
第1面に對向した反射面である第2面を介して外界象を
観察する場合、この2面の中少なくとも1面は観察者視
軸に対して偏心あるいは傾いた面であるため、各面高
によって異なる偏ったパワーを有するレンズを通して外界
を観察しているとの同様になる。そこで、外界光に対し
て上記の2面で発生する偏ったパワーを打ち消す作用を
有する第2光学素子を接眼光学系の外周側に配置するこ
とより、観察者はより自然で広範囲な外界象を観察する
ことができる。したがって、危険防止と緊急時対応がで
きる、安全な画像表示装置を提供することができる。

[0.086] この場合、接眼光学系は、薄板で形成され
る空間を屈折率が1より大きい媒質で満され、その4
面は、観察者眼鏡側に位置している屈折率が1より大きい
面に向し第1面に對向した反射面である第2面、第
1面に對向し第2面に對向した反射面である第3面、画
像表示素子に最も近接している屈折面である第4面で構
成され、少なくとも1面が観察者視軸に対して偏心する
かあるいは傾いた面を含む偏心プリズムからなつていて
もよい。接眼光学系がこのように4面で構成されている
場合、第1面と第2面を通過した外界光によって外界を
観察する。その場合、第2面を経験する領域において
み偏ったパワーを打ち消す作用を有する第2光学素子を
配置することで、接眼光学系全体は大型化せずに付加功
能を実現する事が可能となる。

[0.087] また、第1面と第2面と第2光学素子、若
しくは、第1面と第3面と第2光学素子を介して外界を
観察できるように、少なくとも1つの第2光学素子を第
2面又は第3面の外周側に配置することが望ましい。第
2面の外周側に偏ったパワーを打ち消す作用を有する第

2光学素子を配置することで、電子像を観察する領域と
同一領域において自然な外界象を観察することができ
る。また、同様に、第3面の外周側に偏ったパワーを打
ち消す作用を有する第2光学素子を配置することより電
子像とは異なる領域においても自然な外界を観察でき
る。さらに、2つの第2光学素子を同時に第2面と第3
面の外周側に配置することにより、観察者は第1面と第2
面及び第1面と第3面を通過する外界像を全て観察する
ことが可能である。したがって、電子の屈折角よりも外
界側内部反射面と、前記画像表示素子の発する光束を入
射する屈折面である。

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これが可能である。これにより、危険防止と緊急時の適切な
対応ができる、非常に安全な画像表示装置を提供すること
ができる。

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が可能である。

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[0.088] また、第2光学素子は、外界光に対する第
1面と第2面、若しくは、第1面と第3面のそれぞれの
合成パワーを同時に打ち消す作用を有することが望ま
しい。外界光に対する第1面と第2面、第1面と第3面の
それぞれの合成パワーを同時に打ち消す作用を有する第
2光学素子を1つの光学素子として、接眼光学系の外
周側に配置することで広範囲の外界を観察できる。この
ことによって、合成パワーを打ち消す

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ことができる。

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が可能である。

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が可能である。

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が可能である。

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*に4mmである。

なお、本発明の実施例においては、X方向に均等な光学系として屈折したので、X奇数項の係数は0とした(上記でいえば、 $C_1, C_3, C_5, \dots = 0$)。[0115]なお、後述の構成パラメータ中、データの記載されていない非球面、関する項は0である。屈折率については、d線(波長587.5 nm)に対するものを表記している。長さの単位はmmである。

[0116]実施例1～4、5～17の光路2を含むY軸の構成パラメーター及び条件式の値を示す。実施例7、8は実施例3と同じであるので省く。また、実施例10、11の画像表示素子観察時構成パラメーターは実施例5と同じであるので、外界観察時構成パラメーターを示す。また、実施例12の画像表示素子観察時構成パラメーターを実施例12(1)として、外界観察時構成パラメーターを実施例12(2)として示す。

に示す。実施例1～11、13、14の観察屈角は、水平屈角30.0°、垂直屈角22.7°、実施例12～16の水平屈角30.0°、垂直屈角22.7°、実施例1～5の観察屈角は、水平屈角35.3°、垂直屈角40.0°、実施例6～9の観察屈角は、水平屈角35.0°、垂直屈角40.0°、実施例10～16共*

[0117]以下に、上記実施例1～6、9～14、17の構成パラメーター及び条件式の値を示す。実施例7、8は実施例3と同じであるので省く。また、実施例10、11の画像表示素子観察時構成パラメーターは実施例5と同じであるので、外界観察時構成パラメーターを示す。また、実施例12の画像表示素子観察時構成パラメーターを実施例12(1)として、外界観察時構成パラメーターを実施例12(2)として示す。

(1) $\theta_{\text{r}} = 43.85^\circ$

(3) $\phi_{\text{r}} : (yz) = 0 \quad (1/\text{mm})$
 $\phi_{\text{r}} : (xz) = 0 \quad (1/\text{mm})$

[0118]

[0119]

実施例1
屈筋号 曲率半径 両側 屈折率 アップベ数
(屈心量)
(傾き角)

1 ∞ (屈)

2 ASPH ∞ Y 1.5554 θ 4.44°
(1ST SP) K 0.0000 Z 37.01

3 ANAM R_r -147.51 Y 3.041 θ -17.71°
(1ND SP) R_s -117.07 Y 3.041 θ -17.71°
(1IP) K_r -5.4537 Z 57.131

4 R_r -5.0000 $\times 10^{-10}$ Y 1.5554
(1IP) K_r -0.2158 Z 37.01

5 R_r 3.618 $\times 10^{-10}$ Y 1.5554 θ 4.44°
(1IP) K_r 1.2600 $\times 10^{-13}$ Z 37.01

6 R_r 4.934 $\times 10^{-13}$ Y 1.5554 θ 4.44°
(1IP) K_r -1.1848 $\times 10^{+1}$ Z 37.01

7 P_r 1.3791 $\times 10^{-1}$ Y 1.5554 θ 4.44°
(1IP) K_r 3.3074 $\times 10^{-1}$ Z 37.01

8 P_r 0.0000 Y 1.5554 θ 4.44°
(1IP) K_r 0.0000 Z 37.01

9 P_r ∞ Y 1.5554 θ 4.44°
(1IP) K_r 0.0000 Z 37.01

[0120]
(画像表示面)
自由曲面①

C₀ -4.3507 $\times 10^{-4}$ C₁ -1.3110 $\times 10^{-3}$ C₂ -7.2046 $\times 10^{-4}$
C₀ -1.4070 $\times 10^{-4}$ C₁ -5.7449 $\times 10^{-3}$ C₂ -7.6285 $\times 10^{-4}$
C₀ 2.1344 $\times 10^{-4}$ C₁ -7.4711 $\times 10^{-3}$ C₂ -1.9357 $\times 10^{-4}$
C₀ 1.3399 $\times 10^{-4}$

[0121]
(画像表示面)
自由曲面②

C₀ -4.4971 $\times 10^{-3}$ C₁ -1.5757 $\times 10^{-2}$ C₂ -6.4211 $\times 10^{-3}$
C₀ -4.6197 $\times 10^{-3}$ C₁ -3.1115 $\times 10^{-2}$ C₂ -4.8891 $\times 10^{-3}$
C₀ -3.1170 $\times 10^{-3}$ C₁ -1.3015 $\times 10^{-2}$ C₂ -3.5112 $\times 10^{-3}$
C₀ -2.4100 $\times 10^{-3}$ C₁ -4.2104 $\times 10^{-2}$

C₀ -1.1971 $\times 10^{-3}$ 自由曲面③

C₀ -5.302 Y 41.210 θ -55.11°
(1IP) K_r 46.005 Z 47.707

K_r 1.9910 Y 41.210 θ -55.11°
(1IP) K_r -0.1607 Z 47.707

R_r 1.1694 $\times 10^{-7}$ 自由曲面④

*に4mmである。

[0122]以下に、上記実施例1～6、9～14、17の構成パラメーター及び条件式の値を示す。実施例7、8は実施例3と同じであるので省く。また、実施例10、11の画像表示素子観察時構成パラメーターは実施例5と同じであるので、外界観察時構成パラメーターを示す。また、実施例12の画像表示素子観察時構成パラメーターを実施例12(1)として、外界観察時構成パラメーターを実施例12(2)として示す。

に示す。実施例1～11、13、14の観察屈角は、水平屈角30.0°、垂直屈角22.7°、実施例12～16の水平屈角30.0°、垂直屈角22.7°、実施例1～5の観察屈角は、水平屈角35.3°、垂直屈角40.0°、実施例6～9の観察屈角は、水平屈角35.0°、垂直屈角40.0°、実施例10～16共*

[0123]以下に、上記実施例1～6、9～14、17の構成パラメーター及び条件式の値を示す。実施例7、8は実施例3と同じであるので省く。また、実施例10、11の画像表示素子観察時構成パラメーターは実施例5と同じであるので、外界観察時構成パラメーターを示す。また、実施例12の画像表示素子観察時構成パラメーターを実施例12(1)として、外界観察時構成パラメーターを実施例12(2)として示す。

(1) $\theta_{\text{r}} = 43.85^\circ$

(3) $\phi_{\text{r}} : (yz) = 0 \quad (1/\text{mm})$
 $\phi_{\text{r}} : (xz) = 0 \quad (1/\text{mm})$

[0124]

実施例2
屈筋号 曲率半径 両側 屈折率 アップベ数
(屈心量)
(傾き角)

1 ∞ (屈)

2 自由曲面① Y 6.738 θ -40.43°
(1ST SP) Z 36.234

3 自由曲面② Y 0.000 θ -21.31°
(1IP) Z 47.732

4 自由曲面③ Y 0.000 θ -4.43°
(1IP) Z 51.303

5 自由曲面④ Y 1.5000 θ 4.44°
(1IP) Z 36.234

6 自由曲面⑤ Y 1.5000 θ 4.44°
(1IP) Z 43.146

7 ∞ Y 37.034 θ -42.31°
(1IP) Z 43.146

8 ∞ Y 37.034 θ -31.45°
(1IP) Z 41.032

[0125]
(画像表示面)
自由曲面①

C₀ -1.4070 $\times 10^{-4}$ C₁ -5.7449 $\times 10^{-3}$ C₂ -7.6285 $\times 10^{-4}$

C₀ 2.1344 $\times 10^{-4}$ C₁ -7.4711 $\times 10^{-3}$ C₂ -1.9357 $\times 10^{-4}$

C₀ 1.3399 $\times 10^{-4}$ C₁ -4.2104 $\times 10^{-2}$

C₀ -1.1971 $\times 10^{-3}$ 自由曲面③

C₀ -5.302 Y 41.210 θ -55.11°
(1IP) K_r 46.005 Z 47.707

K_r 1.9910 Y 41.210 θ -55.11°
(1IP) K_r -0.1607 Z 47.707

R_r 1.1694 $\times 10^{-7}$ 自由曲面④

(1)

特許平10-307263

(1)

特許平10-307263

実施例4	曲率半径 面番号	曲率半径 面番号	屈折率 (屈心量)	屈折率 (屈心量)
1	∞ (屈)	∞ (屈)	1.5154	56.15
2	ANAM R _r -141.348	ANAM R _r -151.768	Y 5.082	θ -3.64°
3	ANAM R _r -143.113 (RFL) K _r 0.3713	ANAM R _r -143.213 (RFL) K _r -1.8942	Z 32.316	
4	∞ (屈)	∞ (屈)	1.5154	56.15
5	ANAM R _r -151.768 (RFL) K _r -0.1181	ANAM R _r -151.768 (RFL) K _r -3.0463	Y 27.149	θ -11.34°
6	∞ (屈)	∞ (屈)	1.5154	56.15
7	∞ (屈)	∞ (屈)	1.5154	56.15

(1)

特許平10-307263

(1)

特許平10-307263

実施例3	曲率半径 面番号	曲率半径 面番号	屈折率 (屈心量)	屈折率 (屈心量)
1	∞ (屈)	∞ (屈)	1.5154	56.15
2	ANAM R _r -141.348 (IST SF) Z 37.345	ANAM R _r -151.768 (IST SF) P _r -1.3978	Y 5.082	θ -3.64°
3	ANAM R _r -143.113 (RFL) K _r 0.3713	ANAM R _r -143.213 (RFL) K _r -1.8942	Z 32.316	
4	∞ (屈)	∞ (屈)	1.5154	56.15
5	ANAM R _r -151.768 (RFL) K _r -0.1181	ANAM R _r -151.768 (RFL) K _r -3.0463	Y 27.149	θ -11.34°
6	∞ (屈)	∞ (屈)	1.5154	56.15
7	∞ (屈)	∞ (屈)	1.5154	56.15

(1)

特許平10-307263

(1)

特許平10-307263

実施例2	曲率半径 面番号	曲率半径 面番号	屈折率 (屈心量)	屈折率 (屈心量)
1	∞ (屈)	∞ (屈)	1.5154	56.15
2	ANAM R _r -141.348 (IST SF) Z 37.345	ANAM R _r -151.768 (IST SF) P _r -1.3978	Y 5.082	θ -3.64°
3	ANAM R _r -143.113 (RFL) K _r 0.3713	ANAM R _r -143.213 (RFL) K _r -1.8942	Z 32.316	
4	∞ (屈)	∞ (屈)	1.5154	56.15
5	ANAM R _r -151.768 (RFL) K _r -0.1181	ANAM R _r -151.768 (RFL) K _r -3.0463	Y 27.149	θ -11.34°
6	∞ (屈)	∞ (屈)	1.5154	56.15
7	∞ (屈)	∞ (屈)	1.5154	56.15

(1)

特許平10-307263

(1)

特許平10-307263

実施例1	曲率半径 面番号	曲率半径 面番号	屈折率 (屈心量)	屈折率 (屈心量)
1	∞ (屈)	∞ (屈)	1.5154	56.15
2	ANAM R _r -141.348 (IST SF) Z 37.345	ANAM R _r -151.768 (IST SF) P _r -1.3978	Y 5.082	θ -3.64°
3	ANAM R _r -143.113 (RFL) K _r 0.3713	ANAM R _r -143.213 (RFL) K _r -1.8942	Z 32.316	
4	∞ (屈)	∞ (屈)	1.5154	56.15
5	ANAM R _r -151.768 (RFL) K _r -0.1181	ANAM R _r -151.768 (RFL) K _r -3.0463	Y 27.149	θ -11.34°
6	∞ (屈)	∞ (屈)	1.5154	56.15
7	∞ (屈)	∞ (屈)	1.5154	56.15

(1)

特許平10-307263

(1)

特許平10-307263

[0120] (画廊表示面)
 (1) $\theta_{r1} = 4.8^\circ, 44.4^\circ$
 (3) $\phi_{r1} (y z) = 0 \text{ (1/mm)}$
 $\phi_{r1} (x z) = -0.0072 \text{ (1/mm)}$

[0121]

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6 ANM	R _x	71.443	Y	47.311	θ	-41.14°		
(4TH SF)	R _x	38.167	Z	43.914				
K _x	-1.0213							
K _x	-7.8305							
R _x	-1.504 × 10 ⁻⁷							
R _x	-5.8510 × 10 ⁻⁹							
R _x	5.8345 × 10 ⁻⁹							
R _x	1.9111 × 10 ⁻⁹							
P _x	-1.4518							
P _x	1.1114 × 10 ⁻⁹							
P _x	1.0220 × 10 ⁻⁹							
P _x	-1.4518							
7		∞	Y	42.878	θ	-11.34°		
			Z	30.111				
(回転表示面)								
(1) θ _{rs} =42.75°								
(3) φ _{rs} (yz)=0. 0.008 (1/mm)								
φ _{rs} (xz)=-0. 0.001 (1/mm)								
[0122]								
実施例5	面番号	曲率半径	屈折率	屈折率 (屈心量)	曲率半径	屈折率 (屈心量)	曲率半径	屈折率 (屈心量)
1	∞ (屈)		1.5154	\$6.15	1	∞ (屈)	Y	0.000 θ 10.00°
2	(1ST SF)	-104.051	Y	2.510 θ -7.01°	2	∞	Z	0.000 \$6.15
			Z	33.57				
3	ANM	R _r	-64.751	1.5154	\$6.15	3	∞	1.5154
(4TH SF)	R _r	-67.004	Y	-19.747 θ -48.41°		(反屈面から)	Y	0.000 θ 0.00°
(REFL)	K _r	-1.3114	Z	30.111		Z	1.5154	
K _r	0.1944							
R _r	1.4430 × 10 ⁻¹⁰							
R _r	-1.1189 × 10 ⁻¹⁰							
R _r	-2.4492 × 10 ⁻⁹							
R _r	1.4084 × 10 ⁻⁹							
P _r	-1.7774 × 10 ⁻¹¹							
P _r	5.3045 × 10 ⁻¹¹							
P _r	-4.1468							
P _r	1.0048 × 10 ⁻¹¹							
4		-104.051	Y	1.5154	\$6.15	5	∞	1.5154
(1ST SF)			Z	2.510 θ -7.01°		(反屈面から)	Y	0.000 θ 0.00°
(REFL)			Z	33.57		Z	40.415	
5 ANM	R _r	-3101.935	Y	-37.487 θ 4.95°		6	∞	1.5154
(4TH SF)	R _r	1243.857	Z	53.061				\$6.15
(REFL)	K _r	0.0000						
K _r	0.0000							
R _r	1.7127 × 10 ⁻⁸							
R _r	1.2246 × 10 ⁻⁸							
R _r	-1.5958 × 10 ⁻⁸							
P _r	3.1613 × 10 ⁻⁸							
7	ANM	R _r	70.481			7	ANM	R _r
(4TH SF)	R _r	41.816				(4TH SF)	R _r	70.481
K _r	6.088					K _r	6.088	
K _r	7.138					R _r	1.635 × 10 ⁻⁸	
R _r	1.635 × 10 ⁻⁸					R _r	1.635 × 10 ⁻⁸	
R _r	1.635 × 10 ⁻⁸							
R _r	-3.4116 × 10 ⁻⁹							
R _r	-7.2147 × 10 ⁻⁹							
P _r	3.1613 × 10 ⁻⁸							

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2

2

(画像表示面)	8
(1) $\theta_{xz} = 46.7^\circ$	P ₁ , 3.8877
(3) $\phi_{xz}(yz) = 0$ (1/mm)	P ₃ , 1.001×10^{-1}
$\phi_{xz}(xz) = 0$ (1/mm)	P ₄ , 1.1138×10^{-1}
	∞

$$\begin{array}{ll} Y & 40, 634 \\ \theta & -3, 0 \\ Z & 30, 403 \end{array}$$

$$\phi_{11}(yz) = 0 \quad (1/\text{mm})$$

$$\phi_{11}(xz) = 0 \quad (1/\text{mm})$$

[0124]

	P ₃	P ₄
P ₃	-4.1468	
P ₄	1.0048 × 10 ⁻¹	

曲率半径	圓周	屈折率 (屈心度)	アッペ散 (散き度)
面番号	実施例9		

	∞ (mm)	γ	0.000	θ
2	∞	Z	0.000	
(仮想面)			1.514	51.15°
3	-221.433	(仮想面から)		
(IST SP)				
Y	0.000	θ		

	K	0.0000
A	2.0650×10^{-4}	
B	-4.2780×10^{-10}	
C	3.2181×10^{-4}	
D	2.1156×10^{-10}	

実施例 11 面番号	曲率半径	開閉	屈折率 ($\eta_{\text{水}}/\eta_{\text{空気}}$)	アッペ数 ($\theta_{\text{引き角}}$)
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5 ((ST ST) (m.s.t))	-221.433		
		Z 46.157	\$6.15
		1.5154	
		(仮想面) Y 0.000	θ 0.000

	1	∞ (III)	1.5154	51.15
	2	-101.651	2.5140	θ
(IST SP)			31.127	-7.01°
Z	Z			

9	(医療用語)	(ASME)	(ANSI)	-403.44-
Z	5.517	0.00	θ	Y
Z	5.517	0.00	θ	Y
Z	5.517	0.00	θ	Y
Z	5.517	0.00	θ	Y

(IND SP)	R _x	-42.004	Z	30.166
(EFLU)	K _r	-1.364		
	K _x	0.184		
R ₁		1.4430×10^{-10}		

R_1	-1.1189×10^{-10}
R_2	-7.4892×10^{-11}
R_3	1.4004×10^{-11}
R_4	-2.7674×10^{-11}
P_1	

$$\begin{aligned}
 (1) \quad & \theta_{zz} = 4.68^\circ \\
 (3) \quad & \phi_{11}(yz) = 0.00024 \text{ (1/mm)} \\
 \phi_{11}(xz) = & 0.00024 \text{ (1/mm)} \quad 40
 \end{aligned}$$

面号	曲率半径	間隔	屈折率 (偏心量)	アップ (傾き)
DATA001	曲率半径	間隔	屈折率 (偏心量)	アップ (傾き)

5
 ∞
 (フレネルレンズ第2面)
 K 0.0000
 A 4.4111×10^{-4}
 B -1.0534×10^{-3}

3	AHAM	R _a	-54.751	V	-18.147	θ	-16.1
(100 S _p)	R _a	-54.006		Z	30.167		
(BSPU)	K _a	-1.3614					

(45) 特開平10-307263
 (フレネルレンズ第1面)
 Y 45.03 θ -11.17°
 Z 45.000

(43) 実施例12 (1)

面番号	曲率半径	屈折率	屈折率 (屈心量)	アッペ数 (傾き角)
1	∞ (屈)			
2	自由曲面①	Y	13.93	θ 4.41°
(1ST SP)		Z	33.974	
3	自由曲面②	Y	1.5154	56.15°
(2ND SP)		Z	49.331	
4	自由曲面①	Y	1.5154	56.15°
(1ST SP)		Z	33.974	
5	自由曲面③	Y	27.094	θ 79.39°
(3RD SP)		Z	35.215	
6	∞	Y	21.208	θ 46.34°
(画像表示面)		Z	46.310	
C ₁	-3.6151×10 ⁻³	C ₁	-3.1701×10 ⁻³	C ₁ -7.5534×10 ⁻¹
C ₁₀	-3.5170×10 ⁻⁴	C ₁₁	1.5154×10 ⁻⁴	C ₁₁ 1.3359×10 ⁻⁴
C ₁₄	1.7146×10 ⁻⁷	C ₁₅	-3.0018×10 ⁻⁹	C ₁₅ 1.7446×10 ⁻⁹
C ₁₅	-2.0581×10 ⁻⁹	C ₁₆	3.8718×10 ⁻¹⁰	C ₁₆ -3.8718×10 ⁻¹⁰
C ₁₇	-3.8718×10 ⁻¹⁰	C ₁₈	1.4081×10 ⁻¹⁰	C ₁₈ 1.4081×10 ⁻¹⁰
C ₁₈	-3.8718×10 ⁻¹⁰	C ₁₉	4.3101×10 ⁻¹¹	C ₁₉ 4.3101×10 ⁻¹¹
C ₁₉	-1.4081×10 ⁻¹¹	C ₂₀	7.4913×10 ⁻¹¹	C ₂₀ -7.4913×10 ⁻¹¹
C ₂₁	7.4913×10 ⁻¹¹	C ₂₂	1.4116×10 ⁻¹¹	C ₂₂ 1.4116×10 ⁻¹¹
C ₂₂	-7.4913×10 ⁻¹¹	C ₂₃	-1.0055×10 ⁻¹¹	C ₂₃ -1.0055×10 ⁻¹¹
C ₂₃	7.4913×10 ⁻¹¹	C ₂₄	4.3101×10 ⁻¹¹	C ₂₄ 4.3101×10 ⁻¹¹
C ₂₄	-7.4913×10 ⁻¹¹	C ₂₅	1.4116×10 ⁻¹¹	C ₂₅ 1.4116×10 ⁻¹¹
C ₂₅	7.4913×10 ⁻¹¹	C ₂₆	-1.0055×10 ⁻¹¹	C ₂₆ -1.0055×10 ⁻¹¹
C ₂₆	-7.4913×10 ⁻¹¹	C ₂₇	4.3101×10 ⁻¹¹	C ₂₇ 4.3101×10 ⁻¹¹
C ₂₇	7.4913×10 ⁻¹¹	C ₂₈	1.4116×10 ⁻¹¹	C ₂₈ 1.4116×10 ⁻¹¹
C ₂₈	-7.4913×10 ⁻¹¹	C ₂₉	-1.0055×10 ⁻¹¹	C ₂₉ -1.0055×10 ⁻¹¹
C ₂₉	7.4913×10 ⁻¹¹	C ₃₀	4.3101×10 ⁻¹¹	C ₃₀ 4.3101×10 ⁻¹¹
C ₃₀	-7.4913×10 ⁻¹¹	C ₃₁	1.4116×10 ⁻¹¹	C ₃₁ 1.4116×10 ⁻¹¹
C ₃₁	7.4913×10 ⁻¹¹	C ₃₂	-1.0055×10 ⁻¹¹	C ₃₂ -1.0055×10 ⁻¹¹
C ₃₂	-7.4913×10 ⁻¹¹	C ₃₃	4.3101×10 ⁻¹¹	C ₃₃ 4.3101×10 ⁻¹¹
C ₃₃	7.4913×10 ⁻¹¹	C ₃₄	1.4116×10 ⁻¹¹	C ₃₄ 1.4116×10 ⁻¹¹
C ₃₄	-7.4913×10 ⁻¹¹	C ₃₅	-1.0055×10 ⁻¹¹	C ₃₅ -1.0055×10 ⁻¹¹
C ₃₅	7.4913×10 ⁻¹¹	C ₃₆	4.3101×10 ⁻¹¹	C ₃₆ 4.3101×10 ⁻¹¹
C ₃₆	-7.4913×10 ⁻¹¹	C ₃₇	1.4116×10 ⁻¹¹	C ₃₇ 1.4116×10 ⁻¹¹
C ₃₇	7.4913×10 ⁻¹¹	C ₃₈	-1.0055×10 ⁻¹¹	C ₃₈ -1.0055×10 ⁻¹¹
C ₃₈	-7.4913×10 ⁻¹¹	C ₃₉	4.3101×10 ⁻¹¹	C ₃₉ 4.3101×10 ⁻¹¹
C ₃₉	7.4913×10 ⁻¹¹	C ₄₀	1.4116×10 ⁻¹¹	C ₄₀ 1.4116×10 ⁻¹¹
C ₄₀	-7.4913×10 ⁻¹¹	C ₄₁	-1.0055×10 ⁻¹¹	C ₄₁ -1.0055×10 ⁻¹¹
C ₄₁	7.4913×10 ⁻¹¹	C ₄₂	4.3101×10 ⁻¹¹	C ₄₂ 4.3101×10 ⁻¹¹
C ₄₂	-7.4913×10 ⁻¹¹	C ₄₃	1.4116×10 ⁻¹¹	C ₄₃ 1.4116×10 ⁻¹¹
C ₄₃	7.4913×10 ⁻¹¹	C ₄₄	-1.0055×10 ⁻¹¹	C ₄₄ -1.0055×10 ⁻¹¹
C ₄₄	-7.4913×10 ⁻¹¹	C ₄₅	4.3101×10 ⁻¹¹	C ₄₅ 4.3101×10 ⁻¹¹
C ₄₅	7.4913×10 ⁻¹¹	C ₄₆	1.4116×10 ⁻¹¹	C ₄₆ 1.4116×10 ⁻¹¹
C ₄₆	-7.4913×10 ⁻¹¹	C ₄₇	-1.0055×10 ⁻¹¹	C ₄₇ -1.0055×10 ⁻¹¹
C ₄₇	7.4913×10 ⁻¹¹	C ₄₈	4.3101×10 ⁻¹¹	C ₄₈ 4.3101×10 ⁻¹¹
C ₄₈	-7.4913×10 ⁻¹¹	C ₄₉	1.4116×10 ⁻¹¹	C ₄₉ 1.4116×10 ⁻¹¹
C ₄₉	7.4913×10 ⁻¹¹	C ₅₀	-1.0055×10 ⁻¹¹	C ₅₀ -1.0055×10 ⁻¹¹
C ₅₀	-7.4913×10 ⁻¹¹	C ₅₁	4.3101×10 ⁻¹¹	C ₅₁ 4.3101×10 ⁻¹¹
C ₅₁	7.4913×10 ⁻¹¹	C ₅₂	1.4116×10 ⁻¹¹	C ₅₂ 1.4116×10 ⁻¹¹
C ₅₂	-7.4913×10 ⁻¹¹	C ₅₃	-1.0055×10 ⁻¹¹	C ₅₃ -1.0055×10 ⁻¹¹
C ₅₃	7.4913×10 ⁻¹¹	C ₅₄	4.3101×10 ⁻¹¹	C ₅₄ 4.3101×10 ⁻¹¹
C ₅₄	-7.4913×10 ⁻¹¹	C ₅₅	1.4116×10 ⁻¹¹	C ₅₅ 1.4116×10 ⁻¹¹
C ₅₅	7.4913×10 ⁻¹¹	C ₅₆	-1.0055×10 ⁻¹¹	C ₅₆ -1.0055×10 ⁻¹¹
C ₅₆	-7.4913×10 ⁻¹¹	C ₅₇	4.3101×10 ⁻¹¹	C ₅₇ 4.3101×10 ⁻¹¹
C ₅₇	7.4913×10 ⁻¹¹	C ₅₈	1.4116×10 ⁻¹¹	C ₅₈ 1.4116×10 ⁻¹¹
C ₅₈	-7.4913×10 ⁻¹¹	C ₅₉	-1.0055×10 ⁻¹¹	C ₅₉ -1.0055×10 ⁻¹¹
C ₅₉	7.4913×10 ⁻¹¹	C ₆₀	4.3101×10 ⁻¹¹	C ₆₀ 4.3101×10 ⁻¹¹
C ₆₀	-7.4913×10 ⁻¹¹	C ₆₁	1.4116×10 ⁻¹¹	C ₆₁ 1.4116×10 ⁻¹¹
C ₆₁	7.4913×10 ⁻¹¹	C ₆₂	-1.0055×10 ⁻¹¹	C ₆₂ -1.0055×10 ⁻¹¹
C ₆₂	-7.4913×10 ⁻¹¹	C ₆₃	4.3101×10 ⁻¹¹	C ₆₃ 4.3101×10 ⁻¹¹
C ₆₃	7.4913×10 ⁻¹¹	C ₆₄	1.4116×10 ⁻¹¹	C ₆₄ 1.4116×10 ⁻¹¹
C ₆₄	-7.4913×10 ⁻¹¹	C ₆₅	-1.0055×10 ⁻¹¹	C ₆₅ -1.0055×10 ⁻¹¹
C ₆₅	7.4913×10 ⁻¹¹	C ₆₆	4.3101×10 ⁻¹¹	C ₆₆ 4.3101×10 ⁻¹¹
C ₆₆	-7.4913×10 ⁻¹¹	C ₆₇	1.4116×10 ⁻¹¹	C ₆₇ 1.4116×10 ⁻¹¹
C ₆₇	7.4913×10 ⁻¹¹	C ₆₈	-1.0055×10 ⁻¹¹	C ₆₈ -1.0055×10 ⁻¹¹
C ₆₈	-7.4913×10 ⁻¹¹	C ₆₉	4.3101×10 ⁻¹¹	C ₆₉ 4.3101×10 ⁻¹¹
C ₆₉	7.4913×10 ⁻¹¹	C ₇₀	1.4116×10 ⁻¹¹	C ₇₀ 1.4116×10 ⁻¹¹
C ₇₀	-7.4913×10 ⁻¹¹	C ₇₁	-1.0055×10 ⁻¹¹	C ₇₁ -1.0055×10 ⁻¹¹
C ₇₁	7.4913×10 ⁻¹¹	C ₇₂	4.3101×10 ⁻¹¹	C ₇₂ 4.3101×10 ⁻¹¹
C ₇₂	-7.4913×10 ⁻¹¹	C ₇₃	1.4116×10 ⁻¹¹	C ₇₃ 1.4116×10 ⁻¹¹
C ₇₃	7.4913×10 ⁻¹¹	C ₇₄	-1.0055×10 ⁻¹¹	C ₇₄ -1.0055×10 ⁻¹¹
C ₇₄	-7.4913×10 ⁻¹¹	C ₇₅	4.3101×10 ⁻¹¹	C ₇₅ 4.3101×10 ⁻¹¹
C ₇₅	7.4913×10 ⁻¹¹	C ₇₆	1.4116×10 ⁻¹¹	C ₇₆ 1.4116×10 ⁻¹¹
C ₇₆	-7.4913×10 ⁻¹¹	C ₇₇	-1.0055×10 ⁻¹¹	C ₇₇ -1.0055×10 ⁻¹¹
C ₇₇	7.4913×10 ⁻¹¹	C ₇₈	4.3101×10 ⁻¹¹	C ₇₈ 4.3101×10 ⁻¹¹
C ₇₈	-7.4913×10 ⁻¹¹	C ₇₉	1.4116×10 ⁻¹¹	C ₇₉ 1.4116×10 ⁻¹¹
C ₇₉	7.4913×10 ⁻¹¹	C ₈₀	-1.0055×10 ⁻¹¹	C ₈₀ -1.0055×10 ⁻¹¹
C ₈₀	-7.4913×10 ⁻¹¹	C ₈₁	4.3101×10 ⁻¹¹	C ₈₁ 4.3101×10 ⁻¹¹
C ₈₁	7.4913×10 ⁻¹¹	C ₈₂	1.4116×10 ⁻¹¹	C ₈₂ 1.4116×10 ⁻¹¹
C ₈₂	-7.4913×10 ⁻¹¹	C ₈₃	-1.0055×10 ⁻¹¹	C ₈₃ -1.0055×10 ⁻¹¹
C ₈₃	7.4913×10 ⁻¹¹	C ₈₄	4.3101×10 ⁻¹¹	C ₈₄ 4.3101×10 ⁻¹¹
C ₈₄	-7.4913×10 ⁻¹¹	C ₈₅	1.4116×10 ⁻¹¹	C ₈₅ 1.4116×10 ⁻¹¹
C ₈₅	7.4913×10 ⁻¹¹	C ₈₆	-1.0055×10 ⁻¹¹	C ₈₆ -1.0055×10 ⁻¹¹
C ₈₆	-7.4913×10 ⁻¹¹	C ₈₇	4.3101×10 ⁻¹¹	C ₈₇ 4.3101×10 ⁻¹¹
C ₈₇	7.4913×10 ⁻¹¹	C ₈₈	1.4116×10 ⁻¹¹	C ₈₈ 1.4116×10 ⁻¹¹
C ₈₈	-7.4913×10 ⁻¹¹	C ₈₉	-1.0055×10 ⁻¹¹	C ₈₉ -1.0055×10 ⁻¹¹
C ₈₉	7.4913×10 ⁻¹¹	C ₉₀	4.3101×10 ⁻¹¹	C ₉₀ 4.3101×10 ⁻¹¹
C ₉₀	-7.4913×10 ⁻¹¹	C ₉₁	1.4116×10 ⁻¹¹	C ₉₁ 1.4116×10 ⁻¹¹
C ₉₁	7.4913×10 ⁻¹¹	C ₉₂	-1.0055×10 ⁻¹¹	C ₉₂ -1.0055×10 ⁻¹¹
C ₉₂	-7.4913×10 ⁻¹¹	C ₉₃	4.3101×10 ⁻¹¹	C ₉₃ 4.3101×10 ⁻¹¹
C ₉₃	7.4913×10 ⁻¹¹	C ₉₄	1.4116×10 ⁻¹¹	C ₉₄ 1.4116×10 ⁻¹¹
C ₉₄	-7.4913×10 ⁻¹¹	C ₉₅	-1.0055×10 ⁻¹¹	C ₉₅ -1.0055×10 ⁻¹¹
C ₉₅	7.4913×10 ⁻¹¹	C ₉₆	4.3101×10 ⁻¹¹	C ₉₆ 4.3101×10 ⁻¹¹
C ₉₆	-7.4913×10 ⁻¹¹	C ₉₇	1.4116×10 ⁻¹¹	C ₉₇ 1.4116×10 ⁻¹¹
C ₉₇	7.4913×10 ⁻¹¹	C ₉₈	-1.0055×10 ⁻¹¹	C ₉₈ -1.0055×10 ⁻¹¹
C ₉₈	-7.4913×10 ⁻¹¹	C ₉₉	4.3101×10 ⁻¹¹	C ₉₉ 4.3101×10 ⁻¹¹
C ₉₉	7.4913×10 ⁻¹¹	C ₁₀₀	1.4116×10 ⁻¹¹	C ₁₀₀ 1.4116×10 ⁻¹¹
C ₁₀₀	-7.4913×10 ⁻¹¹	C ₁₀₁	-1.0055×10 ⁻¹¹	C ₁₀₁ -1.0055×10 ⁻¹¹
C ₁₀₁	7.4913×10 ⁻¹¹	C ₁₀₂	4.3101×10 ⁻¹¹	C ₁₀₂ 4.3101×10 ⁻¹¹
C ₁₀₂	-7.4913×10 ⁻¹¹	C ₁₀₃	1.4116×10 ⁻¹¹	C ₁₀₃ 1.4116×10 ⁻¹¹
C ₁₀₃	7.4913×10 ⁻¹¹	C ₁₀₄	-1.0055×10 ⁻¹¹	C ₁₀₄ -1.0055×10 ⁻¹¹
C ₁₀₄	-7.4913×10 ⁻¹¹	C ₁₀₅	4.3101×10 ⁻¹¹	C ₁₀₅ 4.3101×10 ⁻¹¹
C ₁₀₅	7.4913×10 ⁻¹¹	C ₁₀₆	1.4116×10 ⁻¹¹	C ₁₀₆ 1.4116×10 ⁻¹¹
C ₁₀₆	-7.4913×10 ⁻¹¹	C ₁₀₇	-1.0055×10 ⁻¹¹	C ₁₀₇ -1.0055×10 ⁻¹¹
C ₁₀₇	7.4913×10 ⁻¹¹	C ₁₀₈	4.3101×10 ⁻¹¹	C ₁₀₈ 4.3101×10 ⁻¹¹
C ₁₀₈	-7.4913×10 ⁻¹¹	C ₁₀₉	1.4116×10 ⁻¹¹	C ₁₀₉ 1.4116×10 ⁻¹¹
C ₁₀₉	7.4913×10 ⁻¹¹	C ₁₁₀	-1.0055×10 ⁻¹¹	C ₁₁₀ -1.0055×10 ⁻¹¹
C ₁₁₀	-7.4913×10 ⁻¹¹	C ₁₁₁	4.3101×10 ⁻¹¹	C ₁₁₁ 4.3101×10 ⁻¹¹
C ₁₁₁	7.4913×10 ⁻¹¹	C ₁₁₂	1.4116×10 ⁻¹¹	C ₁₁₂ 1.4116×10 ⁻¹¹
C ₁₁₂	-7.4913×10 ⁻¹¹	C ₁₁₃	-1.0055×10 ⁻¹¹	C ₁₁₃ -1.0055×10 ⁻¹¹
C ₁₁₃	7.4913×10 ⁻¹¹	C ₁₁₄	4.3101×10 ⁻¹¹	C ₁₁₄ 4.3101×10 ⁻¹¹
C ₁₁₄	-7.4913×10 ⁻¹¹	C ₁₁₅	1.4116×10 ⁻¹¹	C ₁₁₅ 1.4116×10 ⁻¹¹
C ₁₁₅	7.4913×10 ⁻¹¹	C ₁₁₆	-1.0055×10 ⁻¹¹	C ₁₁₆ -1.0055×10 ⁻¹¹
C ₁₁₆	-7.4913×10 ⁻¹¹	C ₁₁₇	4.3101×10 ⁻¹¹	C ₁₁₇ 4.3101×10 ⁻¹¹
C ₁₁₇				

C₁₀ -5.9546×10⁻⁶
C₁₁ -2.2133×10⁻⁴
C₁₂ 1.0400×10⁻⁴

C₁₃ -4.1851×10⁻⁴
C₁₄ 2.0100×10⁻⁴
C₁₅ 0.

[0130]

実施例14

面番号

曲率半径

曲面

屈折率

(屈心量)

アッペ数

(傾き角)

自由曲面○

C₁ -4.9463×10⁻³
C₂ 1.7114×10⁻⁴
C₃ 4.5713×10⁻⁴
C₄ -1.4359×10⁻⁷
C₅ 7.0713×10⁻¹⁰
C₆ 5.3774×10⁻¹¹
C₇ 1.3611×10⁻¹¹

C₈ -5.1413×10⁻³
C₉ 7.9133×10⁻⁴
C₁₀ 2.6471×10⁻⁴
C₁₁ -1.6453×10⁻⁶
C₁₂ -3.3070×10⁻⁹
C₁₃ 4.1801×10⁻⁹
C₁₄ 1.0101×10⁻⁹
C₁₅ -1.1010×10⁻⁹
C₁₆ -7.3311×10⁻⁹

C₁₇ -5.6519×10⁻³
C₁₈ 1.3112×10⁻⁴
C₁₉ 3.1071×10⁻⁷
C₂₀ -1.4332×10⁻⁹
C₂₁ 4.1313×10⁻⁹
C₂₂ -1.4313×10⁻⁹

C₂₃ 3.0116×10⁻⁹
C₂₄ 1.0133×10⁻⁹
C₂₅ 3.1313×10⁻⁹
C₂₆ -4.1115×10⁻⁹

自由曲面○

*ことは書うまでもない。
[0133] 面対称な自由曲面の他の定義式として、Z
ernike多項式がある。この面の形状は以下のように定義する。その定義式のZ軸がZernike
多項式の軸となる。

[0132] 以上の実施例では、前記定義式(a)、(b)、(c)の非球面、アナモルフィック面、自由曲面で構成したが、次の定義式(d)のように定義したZ
ernike多項式で表される圓形、次の定義式(e)のように定義したX方向に対称な自由曲面での設
計が可能である。つまり、あらゆる定義の曲面が使える。*

X=R×cos(h)
Y=R×sin(h)

Z=D,

+D₁ Rcos(h)+D₂ Rsin(h)
+D₃ R² cos(h)+D₄ R² sin(h)

+D₅ R³ cos(h)+D₆ R³ sin(h)
+D₇ R⁴ cos(h)+D₈ R⁴ sin(h)
+D₉ (6R²-6R²+1)+D₁₀ (4R²-3R²) sin(h)
+D₁₁ R⁵ sin(h)+D₁₂ R⁵ cos(h)
+D₁₃ (5R⁴-4R⁴) cos(h)
+D₁₄ (10R³-12R³+3R) sin(h)
+D₁₅ (5R²-4R²) sin(h)+D₁₆ R⁶ sin(h)
+D₁₇ R⁷ cos(h)+D₁₈ (6R⁵-5R⁵) cos(h)
+D₁₉ (15R⁴-20R⁴+6R⁴) cos(h)
+D₂₀ (20R³-30R³+12R³-1)
+D₂₁ (15R²-20R²+6R²) sin(h)
+D₂₂ (6R⁶-5R⁶) sin(h)+D₂₃ R⁸ sin(h)

(d)
なお、上記においてX方向に対称面として表した。た
だし、D_m (mは2以上の整数)は係数である。※
式に対応して次のように定義できる。
Z=C,
+C, Y+C, |X|
+C, Y'+C, Y|X|+C, X'
+C, Y'+C, Y|X|+C, X'|+C₁₀ YX'+C₁₁ |X'|

[0131]

実施例17

面番号

曲率半径

曲面

屈折率

(屈心量)

アッペ数

(傾き角)

自由曲面○

*ことは書うまでもない。
[0133] 面対称な自由曲面の他の定義式として、Z
ernike多項式がある。この面の形状は以下のように定義する。その定義式のZ軸がZernike
多項式の軸となる。

X=R×cos(h)
Y=R×sin(h)

Z=D,

+D₁ Rcos(h)+D₂ Rsin(h)
+D₃ R² cos(h)+D₄ R² sin(h)
+D₅ R³ cos(h)+D₆ R³ sin(h)
+D₇ R⁴ cos(h)+D₈ R⁴ sin(h)
+D₉ (6R²-6R²+1)+D₁₀ (4R²-3R²) sin(h)

(d)
なお、上記においてX方向に対称面として表した。た
だし、D_m (mは2以上の整数)は係数である。※
式に対応して次のように定義できる。
Z=C,
+C, Y+C, |X|
+C, Y'+C, Y|X|+C, X'
+C, Y'+C, Y|X|+C, X'|+C₁₀ YX'+C₁₁ |X'|

5

11

17

6

11

11

[0155] (15) 上記(12)から(14)の何れか1項において、前記が外観作用は前記第1面と前記第3面の少なくとも一部の領域における合成のパワーが零となるように形成されていることを特徴とする像観察装置。

[0156] (16) 上記(12)から(15)の何れか1項において、前記第1面と前記第3面が曲面にて形成されていることを特徴とする像観察装置。

[0157] (17) 上記(12)から(16)の何 *
-0.5 ≤ φ1 ≤ 0.5 (1/mm)

を満たすことを特徴とする像観察装置。

[0160] (20) 上記(12)から(19)の何れか1項において、前記形成手段部材は、前記像形成手段によって形成された像の観察時及び外界の観察時によつて形成されても同じ位置に固定されているよ

うに形成されていることを特徴とする像観察装置。

[0161] (21) 上記(20)において、前記第1面と前記第3面を通して部分領域別に前記像形成手段からの像と外界像を観察可能であることを特徴とする像観察装置。

[0162] (22) 上記(12)から(19)の何れか1項において、前記形成手段部材は、前記像形成手段によって形成された像の観察時と前記像形成手段部材は、前記第1面と外界の観察時とを併せて形成させた後、前記切替手段は、前記プリズム部材を移動させた後するように形成されてい

ることを特徴とする像観察装置。

[0163] (23) 上記(22)において、前記像形成手段部材は、前記像形成手段によって形成された像を観察する際の前記プリズム部材から観察者眼球に到る光路が、前記第1面と外界の観察時とを併せて形成させた後するように前記プリズム部材を移動させることを特徴とする像観察装置。

[0164] (24) 上記(22)又は(23)において、前記切替手段は、前記プリズム部材を軸上光路の光路を含む面に沿つて可動するようによつて構成されることを特徴とする像観察装置。

[0165] (25) 上記(24)又は(23)において、前記切替手段は、前記プリズム部材を観察者の視軸に垂直方向に移動させる構成を有することを特徴とする像観察装置。

[0166] (26) 上記(22)又は(23)において、前記切替手段は、前記プリズム部材を回転可能となるようによつて構成されることを特徴とする像観察装置。

[0167] (27) 像形成手段と、前記像形成手段によって形成された像を観察領域に導く作用を持つ接続手段と前記接続光学系を観察者眼部に対して位置決めて形成される像を観察領域において、前記接続光学系が少なくともプリズム部材を含み、前記プリズム部材は、その面構成の中、透鏡又は反射の光学作用を持った光学作用面が少なくとも4つ設けられ、かつ、その4つ

*われか1項において、前記第1面と前記第3面とが球面にて形成されていることを特徴とする像観察装置。

[0158] (18) 上記(12)から(14)の何れか1項において、前記第1面と前記第3面が平面にて形成されていることを特徴とする像観察装置。

[0159] (19) 上記(12)から(18)の何れか1項において、前記第1面と前記第3面との位置における合成のパワーをよりとする場合、

2面と前記第3面とを構成する1つの面は、前記第4面に近い領域が第3面として作用し、前記第4面から遠い領域が第2面として作用するよう構成していることを特徴とするプリズム光学系又はプリズム部材。

[0170] (36) 上記(35)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外界像観察部材を構成する複数の面を構成する像観察装置。

[0171] (37) 上記(36)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像観察装置。

[0172] (38) 上記(37)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像観察装置。

[0173] (39) 上記(10)、(14)から(26)、(32)の何れか1項において、前記接続光学系と前記像表示手段と前記接続検出手段とを観察者眼面に保持する作用を持つ保材で構成していることを特徴とする像表示装置。

[0174] (40) 上記(10)、(14)から(26)、(32)、(33)の何れか1項において、前記接続光学系と前記像表示手段と前記接続検出手段とを観察者眼面に保持する作用を持つ保材で構成していることを特徴とする像表示装置。

[0175] (35) 上記(1)～(10)及び(27)～(34)の何れか1項において、前記第2面及び前記第3面とが、光学作用的には別々の面として作用し、かつ、構成的には1つの面にて形成されていることを特徴とするプリズム光学系又はプリズム部材。

[0176] (36) 上記(35)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0177] (37) 上記(36)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0178] (38) 上記(37)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0179] (39) 上記(38)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0180] (40) 上記(39)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0181] (41) 上記(38)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0182] (42) 上記(39)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0183] (43) 上記(40)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0184] (44) 上記(41)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0185] (45) 上記(42)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0186] (46) 上記(43)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0187] (47) 上記(44)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0188] (48) 上記(45)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0189] (49) 上記(46)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0190] (50) 上記(47)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

る支持手段を有することを特徴とする像観察装置。

[0175] (35) 上記(1)～(10)及び(27)～(34)の何れか1項において、前記第2面及び前記第3面とが、光学作用的には別々の面として作用し、かつ、構成的には1つの面にて形成されていることを特徴とするプリズム光学系又はプリズム部材。

[0176] (36) 上記(35)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

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[0178] (38) 上記(37)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0179] (39) 上記(38)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0180] (40) 上記(39)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

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[0184] (44) 上記(42)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

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[0186] (46) 上記(44)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0187] (47) 上記(45)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0188] (48) 上記(46)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0189] (49) 上記(47)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

[0190] (50) 上記(48)において、前記第4面と前記第3面との間に複数の面があり、前記第4面から外側に複数の面を構成する像表示装置。

る。

[0173] 本発明の実施例1～3の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0174] 本発明の実施例1～4の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0175] 本発明の実施例1～5の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0176] 本発明の実施例1～6の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0177] 本発明の実施例1～7の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0178] 本発明の実施例1～8の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0179] 本発明の実施例1～9の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0180] 本発明の実施例1～10の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0181] 本発明の実施例1～11の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0182] 本発明の実施例1～12の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0183] 本発明の実施例1～13の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0184] 本発明の実施例1～14の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0185] 本発明の実施例1～15の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0186] 本発明の実施例1～16の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0187] 本発明の実施例1～17の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0188] 本発明の実施例1～18の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0189] 本発明の実施例1～19の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

[0190] 本発明の実施例1～20の接眼光学系を用いた頭部装着型画像表示装置の単眼用の光学系の断面図である。

3.1…表示装置本体部
3.2…前フレーム
3.3…後フレーム
3.4…鏡面フレーム
3.5…リヤフレート
3.6…リヤカバー
3.9…スピーカ
4.0…ビデオ再生装置
4.0a…スピーカ再生装置部
4.1…ケーブル

NC…コーティング穴
Ob…撮影光学系
Fi…ファインダー光学系
Ca…コンパクトカメラ
GF…前鏡レンズ群
D…明るさ取り
DS…接眼光学系(本発明)
Lt…反射光光学系
P…ボロプリズム
Oc…接眼レンズ

[図6]
[図15]

[図7]
[図13]

[図8]
[図16]

[図1]
[図2]
[図3]

[図4]

[図5]

[図6]

[図7]

[図8]

[図9]

[図10]

[図11]

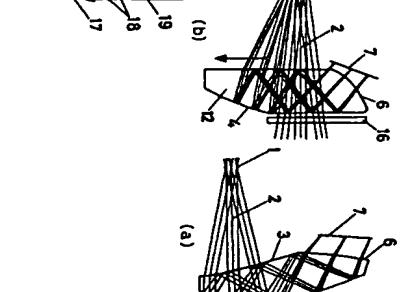
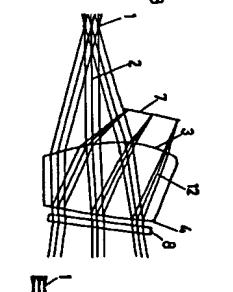
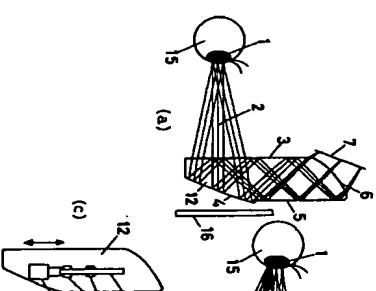
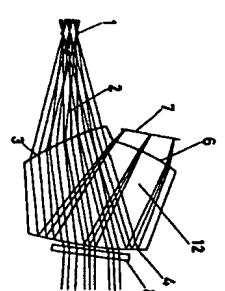
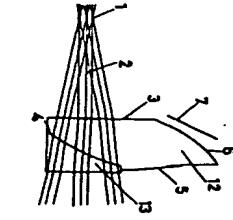
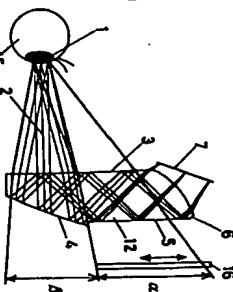
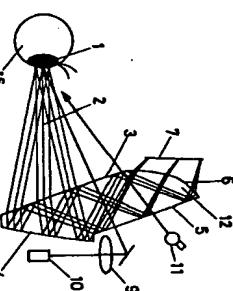
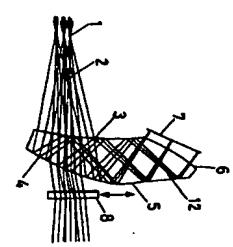
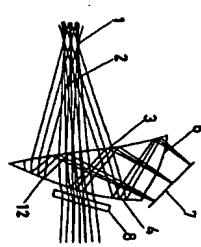
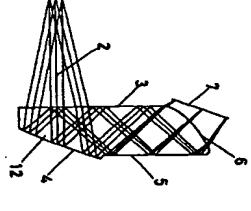
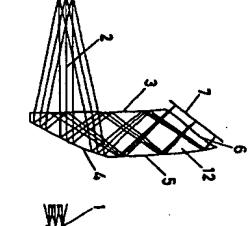
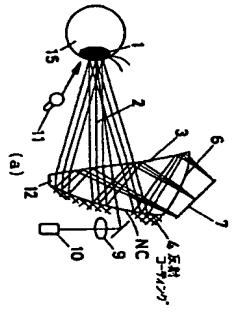
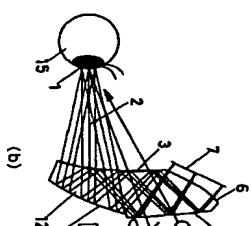
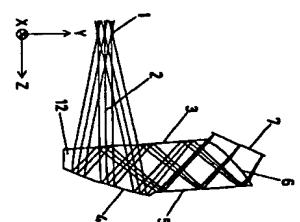
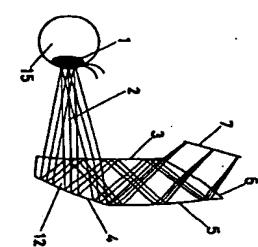
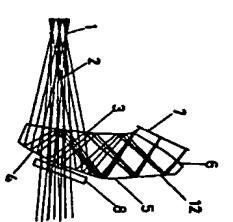
[図12]

[図13]

[図14]

[図15]

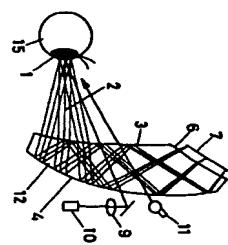
[図16]



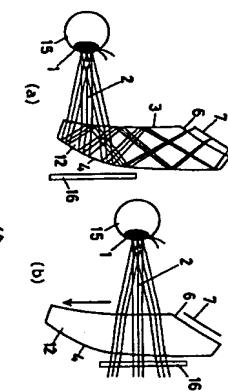
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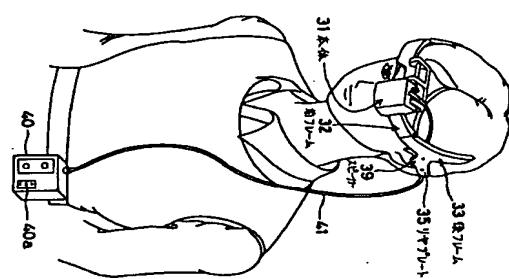
[図17]



[図18]



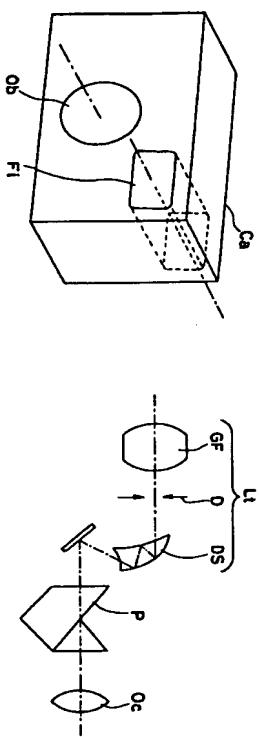
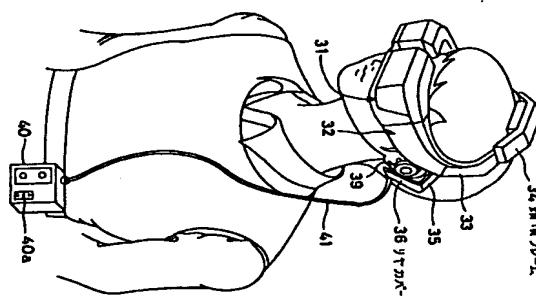
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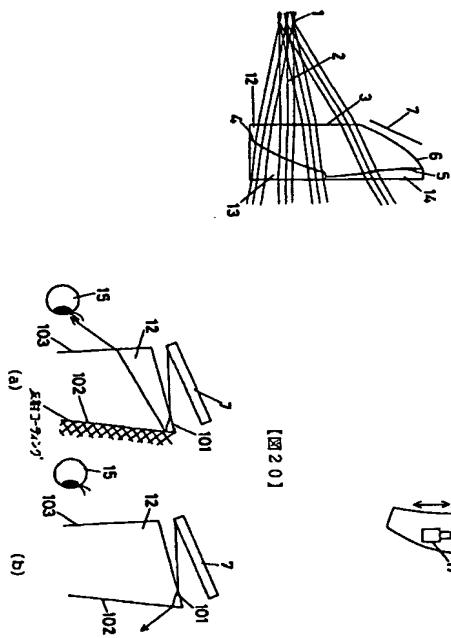
(14)

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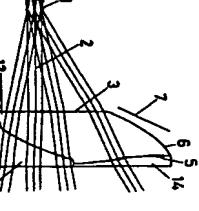
[図22]



[図23]



[図24]



[図19]

JAPANESE LAID-OPEN PATENT APPLICATION

[Claims]

[Claim 1] A prism optical element comprising a plurality of surfaces between which a medium having a refractive index (n) higher than 1 ($n > 1$) is sandwiched,	
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(22)	Date of Filing May 7, 1997

characterized in that the prism optical element has: a first surface having both a transmission property of making a light ray enter the prism optical element or making a light ray exit from the prism optical element, and an internal reflection property in the prism optical element; a second surface disposed so as to be opposed to the first surface with the medium in between, and having an internal reflection property in the prism optical element; a third surface disposed in a position substantially in the vicinity of the second surface so as to be opposed to the first surface with the medium in between, and having an internal reflection property in the prism optical element; and a fourth surface having a transmission property of making the light ray exit from the prism optical element when the first surface has the property of making the light ray enter the prism optical element, and making the light ray enter the prism optical element when the first surface has the property of making the light ray exit from the prism optical element, and making the light ray enter the prism optical element when the first surface has the property of making the light ray exit from the prism optical element, and when the refractive index, to the d-line, of the medium is n_d and the angle of internal reflection of a given light ray at the third surface is θ_a the following expression (1) is satisfied:

$$\sin^{-1}(1/n_d) \leq \theta_a \leq 60^\circ \quad \dots (1)$$

[Claim 2] An image viewing apparatus having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, characterized in that the eyepiece optical system has a prism member having a surface structure provided with at least three surfaces among which a single medium having a refractive index (n) higher than 1 ($n > 1$) is filled, the prism member internally reflects at least three times a light ray emanating from the image forming means, at least two of the at least three internal reflections is total reflection, at least one of the at least two total reflections is performed by a surface disposed on the

viewer side of the single medium of the prism member, the surface is a curved surface that corrects

an aberration caused by the internal reflection by the prism member; and

in order that the outside world can be viewed through at least two of the at least three

surfaces of the prism member, the at least two surfaces are disposed opposed to each other so as to decrease distortion caused when the outside world is viewed with the single medium sandwiched therebetween.

[Claim 3] An image viewing apparatus having image forming means and an eyepiece

optical system that directs an image formed by the image forming means to a viewing eye ball,

characterized in that the eyepiece optical system includes at least a prism member, the

prism member has, in its surface structure, at least four optical property surfaces having an optical

property of transmission or reflection, a space surrounded by the four optical

prism member has, in its surface structure, at least four optical property surfaces having an optical

property of transmission or reflection, a space surrounded by the four optical property surfaces is

filled with a single medium having a refractive index (n) higher than 1 ($n > 1$),

the four optical property surfaces comprise: a first surface having a transmission property

and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a

reflection property and disposed so as to be opposed to the first surface with the medium in between

and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface

having a reflection property and disposed so as to be opposed to the first surface with the medium in

between and to be substantially adjacent to the second surface; and a fourth surface disposed so that

one end thereof is substantially adjacent to the first surface and the other end thereof is substantially

and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a

reflection property and disposed so as to be opposed to the first surface with the medium in between

and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface

having a reflection property and disposed so as to be opposed to the first surface with the medium in

between and to be substantially adjacent to the second surface; and a fourth surface disposed so that

one end thereof is substantially adjacent to the first surface and the other end thereof is substantially

in the vicinity of the third surface,

the prism member is structured so that at least the second surface or the third surface has a

total reflection property, and line of sight detecting means for detecting the viewer's line of sight is

disposed in the vicinity of an area where total reflection by the second surface or the third surface

having the total reflection property is caused.

[Detailed Description of the Invention]

[Technical Field of the Invention] The present invention relates to a prism optical element and an image viewing apparatus, and more particularly, to a head - or face-mounted image display apparatus capable of being held on the viewer's head or face.

[Prior Art] Examples of a heretofore known head - or face-mounted image display apparatus include

[Claim 4] An image viewing apparatus having image forming means and an eyepiece

optical system that directs an image formed by the image forming means to a viewing eye ball,

characterized in that the eyepiece optical system includes at least a prism member,

the prism member has, in its surface structure, at least four optical property surfaces

having an optical property of transmission or reflection, a space surrounded by the four optical

property surfaces is filled with a single medium having a refractive index (n) higher than 1 ($n > 1$),

the four optical property surfaces comprise: a first surface having a transmission property

and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a

reflection property and disposed so as to be opposed to the first surface with the medium in between

and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface

having a reflection property and disposed so as to be opposed to the first surface with the medium in

between and to be substantially adjacent to the second surface; and a fourth surface disposed so that

one end thereof is substantially adjacent to the first surface and the other end thereof is substantially

and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a

reflection property and disposed so as to be opposed to the first surface with the medium in between

and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface

having a reflection property and disposed so as to be opposed to the first surface with the medium in

between and to be substantially adjacent to the second surface; and a fourth surface disposed so that

one end thereof is substantially adjacent to the first surface and the other end thereof is substantially

in the vicinity of the third surface,

the prism member is structured so that at least the second surface or the third surface has a

total reflection property, and line of sight detecting means for detecting the viewer's line of sight is

disposed in the vicinity of an area where total reflection by the second surface or the third surface

having the total reflection property is caused.

one disclosed in Japanese Laid-open Patent Application No. H3-101709. In this image display apparatus, the image displayed on the image display device is transmitted as an aerial image by a relay optical system comprising positive lens elements, the aerial image is enlarged by an eyepiece optical system comprising a concave reflecting mirror, and the enlarged image is projected within the viewer's eye ball.

Examples of another type of conventional image display apparatus is one disclosed in United States Patent No. 4,669,810. In this apparatus, an intermediate image of the image on a CRT is formed through a relay optical system, and the intermediate image is projected onto the viewer's eye by a combiner having a reflection holographic element and a hologram surface.

Examples of yet another type of conventional image display apparatus include one disclosed in United States Patent No. 4,026,641. In this apparatus, the image on the image display device is transmitted to a curved object surface by a transfer element, and the object surface is projected in the air by a toric reflecting surface.

Examples of still another type of conventional image display device include one disclosed in United States Reissued Patent No. 27,356. This apparatus is an eyepiece optical system that projects the object surface onto the exit pupil by a semitransparent concave mirror and a semitransparent plane mirror.

One disclosed in the following are also known: United States Patent No. 4,322,135, United States Patent No. 4,965,724, European Patent No. 0,581,116A2, and Japanese Laid-open Patent Application No. H7-33351.

[Problem to be Solved by the Invention] However, in the image display apparatuses of the type in which the image on the image display device is relayed like the ones disclosed in Japanese Laid-open Patent Application No. H3-101709 and United States Patent No. 4,669,810, since it is necessary to use several lens elements as the relay optical system in addition to the eyepiece optical system irrespective of the form of the eyepiece optical system, the optical path length is large, so that

the optical system is large in size and heavy in weight.

A head-mounted image display apparatus is worn on the human body, particularly on the head. Therefore, when the amount of protrusion of the apparatus from the face is large, the distance from the point at which the apparatus is supported on the head to the center of gravity of the apparatus is long, which results in poor balance when the apparatus is worn. In addition, there is a fear that the apparatus bumps against an object when the viewer wearing the apparatus moves or turns. That is, it is important for head-mounted image display apparatuses to be compact and lightweight. A great factor that decides the size and weight of the apparatus is the optical system structure.

However, when only a normal magnifier is used as the eyepiece optical system, an extremely large amount of aberration is generated and there is no means for correcting it. Although spherical aberration can be corrected to some extent by making the concave surface of the magnifier aspherical, since aberrations such as coma aberration and curvature of field remain, the apparatus cannot be practical when the viewing angle is large. When only a concave mirror is used as the eyepiece optical system, means such that the generated curvature of field is corrected by a conduction element (fiber plate) having a surface curved in accordance with the curvature of field must be used as well as normal optical elements (lens elements and mirrors).

In the type in which the image on the image display device is projected onto the viewer's eye ball by use of a toric reflecting surface like the one disclosed in United States Patent No. 4,026,641, since curvature of field caused by the decentered toric reflecting surface is corrected by curving the object surface itself, it is difficult to use a so-called flat display such as an LCD (liquid crystal display device) as the image display device.

In the coaxial eyepiece optical system that projects the object surface onto the viewer's pupil by use of a semitransparent concave mirror and a semitransparent plane mirror like the one disclosed in United States Reissued Patent No. 27,356, since two semitransparent surfaces are used,

the image brightness decreases to as low as $1/16$ even in theoretical value. In addition, since curvature of field caused by the semitransparent concave mirror is corrected by curving the object surface itself, it is difficult to use a flat display such as an LCD (liquid crystal display device) as the image display device like the conventional example described above.

The present invention is made in view of the above-mentioned prior art problem, and an object thereof is to provide a very-small-size image viewing apparatus that provides a clear viewing image with few distortions and few aberrations even at a wide angle of view, and a prism optical element used for the image viewing apparatus.

[Means for Solving the Problem] In a prism optical element of the present invention achieving the above-mentioned object and comprising a plurality of surfaces between which a medium having a refractive index (n) higher than 1 ($n > 1$) is sandwiched, the prism optical element has: a first surface having both a transmission property of making a light ray enter the prism optical element or making a light ray exit from the prism optical element, and an internal reflection property in the prism optical element; a second surface disposed so as to be opposed to the first surface with the medium in between, and having an internal reflection property in the prism optical element; a third surface disposed in a position substantially in the vicinity of the second surface so as to be opposed to the first surface with the medium in between, and having an internal reflection property in the prism optical element; and a fourth surface having a transmission property of making the light ray exit from the prism optical element when the first surface has the property of making the light ray enter the prism optical element, and making the light ray enter the prism optical element when the first surface has the property of making the light ray exit from the prism optical element, and when the refractive index, to the d-line, of the medium is n_d and the angle of internal reflection of a given light ray at the third surface is θ_{dA} , the following expression (1) is satisfied:

$$\sin^{-1}(1/n_d) \leq \theta_{dA} \leq 60^\circ \quad \dots (1)$$

In the present invention, the structure of the second surface and the third surface is not

limited to the one in which separately designed surfaces are disposed adjacent to each other, but includes a structure using one surface one partial area of which acts as the second surface and another partial area of which acts as the third surface. In that case, needless to say, an overlapping area that acts both the second surface and the third surface may be present because a ray bundle has a width.

In an image viewing apparatus according to the present invention having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system has a prism member having a surface structure provided with at least three surfaces among which a single medium having a refractive index (n) higher than 1 ($n > 1$) is filled, the prism member internally reflects at least three times a light ray emanating from the image forming means, at least two of the at least three internal reflections is total reflection, at least one of the at least two total reflections is performed by a surface disposed on the viewer side of the single medium of the prism member, the surface is a curved surface that corrects an aberration caused by the internal reflection by the prism member, and in order that the outside world can be viewed through at least two of the at least three surfaces of the prism member, the at least two surfaces are disposed opposed to each other so as to decrease distortion caused when the outside world is viewed with the single medium sandwiched therebetween.

In another image viewing apparatus of the present invention having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system includes at least a prism member, the prism member has, in its surface structure, at least four optical property surfaces having an optical property of transmission or reflection, a space surrounded by the four optical property surfaces and a surface other than the four surfaces is filled with a single medium having a refractive index (n) higher than 1 ($n > 1$), the four optical property surfaces comprise: a first surface having a transmission property and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a

reflection property and disposed so as to be opposed to the first surface with the medium in between and to be at least decentered or inclined with respect to the viewer's axis of sighting; a third surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be substantially adjacent to the second surface; and a fourth surface disposed so that one end thereof is substantially adjacent to the first surface and the other end thereof is substantially in the vicinity of the third surface, the prism member is structured so that at least the third surface has a total reflection property; and the first surface, the single medium and the third surface are structured so as to have an outside world viewing property that enables the outside world to be viewed through the first surface, the single medium and the third surface.

In still another image viewing apparatus of the present invention having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system includes at least a prism member, the prism member has, in its surface structure, at least four optical property surfaces having an optical property of transmission or reflection, a space surrounded by the four optical property surfaces is filled with a single medium having a refractive index (n) higher than 1 ($n > 1$), the four optical property surfaces comprise: a first surface having a transmission property and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be at least decentered or inclined with respect to the viewer's axis of sighting; a third surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be substantially adjacent to the second surface; and a fourth surface disposed so that one end thereof is substantially adjacent to the first surface and the other end thereof is substantially in the vicinity of the third surface, the prism member is structured so that at least the second surface or the third surface has a total reflection property, and line of sight detecting means for detecting the viewer's line of sight is disposed in the vicinity of an area where total reflection by the second surface or the third surface

having the total reflection property is caused.

In the present invention, the structure of the second surface and the third surface is not limited to the one in which separately designed surfaces are disposed adjacent to each other, but includes a structure using one surface one partial area of which acts as the second surface and another partial area of which acts as the third surface. In that case, needless to say, an overlapping area that acts both the second surface and the third surface may be present because a ray bundle has a width.

Hereinafter, the structures, actions and effects of the prism optical element, the image viewing apparatus and the image display apparatus of the present invention will be described.

Particularly in the description of the image viewing apparatus and the image display apparatus, for convenience in the optical system design, description will be given based on backward ray tracing in which a light ray is traced from the position of the viewer's pupil to the image display device unless otherwise specified.

In this image viewing apparatus, the effect of bending the optical path is great by a light ray from the image display device (image forming means) being internally reflected three times in the eyepiece optical system, so that a very thin eyepiece optical system is realized. Further, by two of the three internal reflections being total reflection, the area covered with reflective coating is extremely small, and thus, the present invention succeeds in realizing a compact, lightweight and low-cost eyepiece optical system. Further, by two of the three internal reflections being total reflection, generation of a ghost image due to generation of unnecessary light, or decrease in contrast due to flare can be reduced. Normally, in an optical system having internal reflection and filled with an optical medium of a refractive index higher than 1, influences of light exiting from the image display device at a large angle and unnecessary light due to reflection not on the normal light ray path are a problem. According to the present invention, since the area covered with reflective coating is small because of the use of two totally reflecting surfaces, unnecessary light other than the

normal luminous flux that reaches the pupil from the image display device passes through the two internally reflecting surfaces, so that the unnecessary light that reaches the viewer's pupil is significantly reduced.

This action will be detailed with reference to FIG. 20. FIG. 20 is an enlarged view of a portion, on which light from an image display device 7 is incident, of a decentered prism 12 in which a space formed by three surfaces 101, 102 and 103 decentered with respect to the optical axis is filled with a medium having a refractive index higher than 1. Reference numeral 15 represents the viewer's eye ball. Reference numeral 101 represents an incident surface. Reference numeral 102 represents an outside world side reflecting or totally reflecting surface. Reference numeral 103 represents a viewer side refraction or reflecting surface. (a) of FIG. 20 shows a case where the reflecting surface 102 is covered with reflective coating. (b) of FIG. 20 shows a case where the reflecting surface 102 is a totally reflecting surface and is not covered with reflective coating. In the case of (a) of FIG. 20, light exiting from the left side of the image display device 7 at a large angle is incident on the incident surface 101 of the decentered prism 12 to be refracted, is reflected at the reflecting surface 102 covered with reflective coating, and passes through the refraction surface 103 to be incident on the viewer's eye ball 15. Consequently, the viewer sees an unnecessary electronic image in an upper part of the viewer's field of view in addition to the normal image on the image display device 7 (hereinafter, referred to as electronic image), or flare is caused in an upper part.

In the case of (b) of FIG. 20, light exiting from the left side of the image display device 7 at a large angle is incident on the incident surface 101 of the decentered prism 12 to be refracted, and passes through the reflecting surface 102 not covered with reflective coating because the light is incident thereon at an angle not more than a critical angle. Consequently, the light is transmitted toward the side opposite to the viewer and is not incident on the viewer's eye ball 15. That is, a ghost image or flare is not caused.

The above-described action can similarly be caused at a totally reflecting surface in cases other than this example. This can be achieved by setting the luminous flux of a light ray path for viewing the normal electronic image, so as to have an incident angle not less than a critical angle,

and setting other luminous fluxes with exit angles that can cause a ghost or flare, so as to be at an angle not more than the critical angle at the totally reflecting surface. By providing two totally reflecting surfaces, the above-described effect is easily obtained, so that a clear viewing image with no ghost image and little reduction in contrast due to flare can be provided to the viewer.

First, in the prism optical element of the present invention, assuming that it is used as an eyepiece optical system (viewing optical system) of an image viewing apparatus or an image display apparatus, since it comprises a prism member that causes internal reflection at least three times and the prism member is filled with a medium having a refractive index higher than 1, in addition to the effect that the eyepiece optical system can significantly be reduced in thickness by the above-described effect of bending the optical path, the effect of a aberration correction because of the structure in which internal reflection is caused at least three times is great, so that a clear viewing image can be provided in the entire area of the screen. This will be detailed below.

The principal optical power of the prism optical element is provided by the second surface which is a reflecting surface. In this case, since the optical system can be structured with a large radius of curvature compared to a refractive system having the same optical power, aberration generation can be reduced. Since the outside world side reflecting surface is divided into two different surfaces (the second surface and the third surface), the reflected light can be set in a desired direction without depending on the curvature of each surface. Therefore, the optical system can be provided with a shape conforming to the shape of the viewer's face, and the image display device can be disposed with its back facing the viewer side. Particularly, in the case of an image display device requiring a backlight such as an LCD, since the backlight and the electric system are disposed on the viewer side, the image display apparatus does not protrude forward, so that the overall

protrusion of the image display apparatus can be minimized.

Generally, when a concave mirror is disposed so as to be decentered or inclined with respect to the optical axis, aberrations due to decentering that are not caused in coaxial systems are caused. In the prism optical element of the present invention, when it is used for an image viewing apparatus or an image display apparatus, since the second surface is decentered or inclined with respect to the viewer's axis of sighting, aberrations due to decentering are caused. Particularly,

since the axial optical power in a direction along within a plane including the optical path of the axial principal ray (tangential direction) and that in a direction including the axis of sighting and vertical to a plane including the optical path of the axial principal ray (sagittal direction) are different, astigmatism and coma aberration are caused. To correct these decentering aberrations, by at least one of the at least four surfaces constituting the prism optical element being a surface where the optical power in the tangential direction and that in the sagittal direction are different, that is, a rotationally asymmetric surface, the decentering aberrations caused on the second surface can be corrected.

Further, it is effective for the prism optical element to comprise surfaces including only one symmetric surface. When the image display device is disposed on the viewer's axis of sighting (axial principal ray), by at least one of the surfaces constituting the eyepiece optical system being a surface having a symmetric surface in the sagittal direction, a horizontally symmetric viewing image can be projected onto the viewer's eye ball. On the other hand, by providing no symmetric surface in the tangential direction of the surface, the degree of freedom in the tangential direction increases, so that the decentering aberrations caused within the plane including the optical path of the axial principal ray can more excellently be corrected.

When the eyepiece optical system comprises at least four surfaces, the reflection at the first surface can be total reflection. By the first surface disposed immediately before the viewer's pupil being a totally reflecting surface, the area where a light ray exits from the eyepiece optical

system and the internal reflection area can be overlapped with each other. That is, one surface can be provided with two properties, which enables size reduction of the eyepiece optical system.

Moreover, since the above-mentioned effect of reducing ghost or flare by a totally reflecting surface is also obtained on the first surface, a clearer viewing image can be provided.

Further, since reflective coating is provided only on the second surface, manufacturability improves, so that a more inexpensive image display apparatus can be realized.

Moreover, in the prism optical element, when the refractive index, to the d-line, of the medium is n_d and the angle of internal reflection of a given light ray at the third surface is θ_3 , it is desirable to satisfy

$$\sin^{-1}(1/n_d) \leq \theta_3 \leq 60^\circ \quad \dots (1)$$

It is important to satisfy the expression (1). By θ_3 being not less than the lower limit $\sin^{-1}(1/n_d)$, the angle of internal reflection at the third surface is not less than the critical angle, so that the given light ray emanating from the image display device is enabled to be totally reflected at the third surface.

When the angle of reflection at the third surface is too large, the prism optical element is long in a direction vertical to the axis of sighting (tangential direction). Particularly, in the case of a wide-angle image display apparatus, the off-axis ray spreads to such an extent that it cannot reach the first surface at which it is reflected next, so that the prism optical element cannot be realized. Therefore, it is desirable that the given light ray emanating from the image display device be set at not more than 60° which is the upper limit of the expression (1) at the third surface. Further, it is desirable that the following expression (2) be satisfied:

$$\sin^{-1}(1/n_d) \leq \theta_0 \leq 50^\circ \quad \dots (2)$$

Since the third surface is a curved surface inclined or decentered with respect to the optical axis (axial principal ray), the smaller the angle of reflection at this surface is, the smaller the generation of aberrations due to decentering, particularly coma aberration is. Therefore, it is desirable that the

given light ray emanating from the image display device be set at not more than 50° which is the upper limit of the expression (2) at the third surface.

Moreover, to realize an inexpensive image display apparatus, it is important that at least one of the surfaces constituting the prism optical element be a plane. Since the other surfaces can be defined with the at least one plane as the reference, mechanical design and manufacture of the optical system can easily be performed. This enables reduction in processing time, a simplified overall layout of the apparatus and the like, so that a large cost reduction can be realized.

Moreover, similar effects can be obtained by at least one surface being a spherical surface. In that case, since it is easy to define the other surfaces with one spherical surface as the reference, the overall layout of the apparatus and the like are simplified, so that a large cost reduction is enabled.

It is desirable that the refractive index n of the medium of the prism optical element be higher than 1.3.

It is apparent from the description given above that a viewing optical system can be structured by disposing the prism optical element in the viewing optical system.

In that case, the prism optical element may be disposed in the objective lens, or may be disposed in a position that is in the rear of the objective lens and in image erecting means for erecting an object image formed by the objective lens. In the latter, the prism optical element may be provided with both an image erecting property and an eyepiece lens property.

Moreover, the prism optical element of the present invention may be used as a head-mounted image display apparatus having image forming means comprising an LCD (liquid crystal display device) or a CRT disposed so as to be opposed to the fourth surface of the above-described prism optical element, or image forming means comprising an LCD, a CRT or the like relayed by a relay optical system, and a holding member that holds the prism optical element and the image forming means on the viewer's face, wherein a luminous flux emanating from the

image forming means is, in the order of optical paths in the prism optical element, incident on the fourth surface, reflected at the third surface, reflected at the first surface, reflected at the second surface, and exits from the first surface.

In the present invention, one surface may be used both as the second surface and the third surface. In that case, since the physical number of surfaces can be reduced by one, the process can be simplified in optical design and in prism manufacture, which contributes to mass productivity and price reduction. Further, it is desirable that physically one surface having both the property of the second surface and the property of the third surface be used both as the second and the third surfaces and the areas in which the luminous flux is internally reflected be set so as to overlap each other, because size reduction of the prism member can be realized.

Moreover, in an image viewing apparatus of the present invention having image forming

means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system has a prism member having a surface structure provided with at least three surfaces among which a single medium having a refractive index (n) higher than 1 ($n > 1$) is filled, the prism member internally reflects at least three times a light ray emanating from the image forming means, at least two of the at least three internal reflections is total reflection, at least one of the at least two total reflections is performed by a surface disposed on the viewer side of the single medium of the prism member, the surface is a curved surface that corrects an aberration caused by the internal reflection by the prism member, and in order that the outside world can be viewed through at least two of the at least three surfaces of the prism member, the at least two surfaces are disposed opposed to each other so as to decrease distortion caused when the outside world is viewed with the single medium sandwiched therebetween.

In the image viewing apparatus of the present invention, since a third surface 5 is a totally reflecting surface and is not covered with reflective coating, the outside world light passing through the third surface 5 and a first surface 3 reaches the viewer's eye ball 15. Consequently, the outside

world can be viewed in an area α different from the electronic image viewing area β . That the viewer can view the outside world image and the electronic image in different partial areas as mentioned above indicates, for example, that the viewer can simultaneously view the outside world in an upper area and the electronic image in a lower area in the viewer's field of view. The different partial areas may be areas arranged in any direction and parts such as upper and lower areas or left and right areas as long as the viewer can view the two images in different partial areas, respectively.

By providing such a function, the viewer can recognize the outside world while wearing the image display apparatus, so that a safe image display apparatus can be provided that can prevent danger and deal with emergencies. As a result, the area of application as an image display apparatus is widened.

In the image forming apparatus, it is desirable that the image forming means be an image display device (one relayed by the relay optical system is not predetermined) such as an LCD or a CRT of which image formed screen is disposed so as to be opposed to the fourth surface and the second surface be a curved surface.

Moreover, the image forming apparatus can be structured as a head-mounted image display apparatus by providing a holding member that holds the image display device and the eyepiece optical system in front of the viewer's eye ball, and forming the prism member so that the luminous flux emanating from the image display device is incident on the fourth surface, the incident luminous flux is reflected at the third surface, the reflected luminous flux is reflected at the first surface, the reflected luminous flux is reflected at the second surface and the reflected luminous flux exits from the first surface.

Moreover, in the image viewing apparatus, it is desirable that the prism member can be fixed in the same position both when an image formed by the image forming means is viewed and when the outside world image is viewed, and in that case, as described below with reference to FIG. 7, the image from the image forming means and the outside world image can be viewed in different

partial areas through the first surface and the third surface.

The prism member may be provided with switching means for switching between viewing of an image formed by the image forming means and viewing of the outside world image, and be moved by the switching means.

That is, by moving the prism member so that the first surface of the eyepiece optical system disposed immediately before the viewer's eye ball and the third surface disposed on the outside world side and totally reflecting part of the principal ray are in the vicinity of the viewer's axis of sight, the outside world image can be viewed in the periphery of the axis of sight when the viewer faces straight forward, that is, in the vicinity of the center of the field of view, so that the viewer can recognize the outside world before his eyes while wearing the image display apparatus. Consequently, an image display apparatus ensuring safety can be realized.

Moreover, in a structure where the electronic image is kept displayed, by moving and returning the eyepiece optical system, the outside world image and the electronic image can be recognized while switching therebetween is made, so that the area of application is widened.

In this case, it is desirable for the switching means to move the prism member so that the optical path from the prism member to the viewer's eye ball when an image formed by the image forming means is viewed substantially coincides with the optical path from the prism member to the viewer's eye ball when the outside world image is viewed.

Moreover, in a structure where the prism member is moved in a direction along a plane including the optical path of the axial principal ray, since the prism member is linearly moved, the moving mechanism and the overall layout of the apparatus are simplified, so that an inexpensive image display apparatus can be realized.

Moreover, in a structure where the prism member is movable in a direction vertical to the axis of sight, since not only the overall layout of the apparatus and the moving mechanism are simplified but also the amount of forward protrusion from the viewer is the same even after the

eyepiece optical system is moved, a small -size and compact image display apparatus can be provided.

Moreover, in a structure where the prism member is rotatable, since the outside world can be viewed by moving the prism member with a simple rotating mechanism, the mechanism itself is inexpensive, and further, in a structure where the prism members on the left and on the right are simultaneously rotated, the outside world can be recognized with both eyes, so that safety increases and the layout of the apparatus can be realized with a simple structure.

Moreover, in another image viewing apparatus of the present invention having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system includes at least a prism member, the prism member has, in its surface structure, at least four optical property surfaces having an optical property of transmission or reflection, a space surrounded by the four optical property surfaces and a surface other than the four surfaces is filled with a single medium having a refractive index (n) higher than 1 (no 1), the four optical property surfaces comprise: a first surface having a transmission property and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be substantially adjacent to the second surface; and a fourth surface disposed so that one end thereof is substantially adjacent to the first surface and the other end thereof is substantially in the vicinity of the third surface, the prism member is structured so that at least the third surface has a total reflection property, and the first surface, the single medium and the third surface are structured so as to have an outside world viewing property that enables the outside world to be viewed through the first surface, the single medium and the third surface. In this case, the surface other than the four optical property surfaces is a prism side surface or a cut surface having no optical

property.

These image viewing apparatuses are structured so that the outside world can be viewed through a surface disposed immediately before the viewer's eye ball and a surface disposed on the outside world side of the eyepiece optical system. This action and effect will be described with reference to FIG. 7. FIG. 7 is a cross-sectional view of a decentered prism 12 in which a space formed by four surfaces 3, 4, 5 and 6 decentered with respect to the optical axis is filled with a medium having a refractive index higher than 1. In the figure, reference numeral 1 represents the viewer's eye, reference numeral 2 represents the viewer's axis of sighting, reference numeral 3 represents a first surface of an eyepiece optical system 12, reference numeral 4 represents a second surface, reference numeral 5 represents a third surface, reference numeral 6 represents a fourth surface, reference numeral 7 represents an image display device, reference numeral 12 represents the eyepiece optical system, reference numeral 15 represents the viewer's eye ball, and reference numeral 16 represents an optical filter. The actual light ray path from the image display device 7 is such that the light ray emanating from the image display device 7 is incident on the fourth surface 6 of the eyepiece optical system 12, totally reflected at the third surface 5, totally reflected at the first surface 3, reflected at the second surface 4, and again passes through the first surface to project an image onto the viewer's eye ball 15 with the viewer's pupil 1 as the exit pupil.

In the image viewing apparatus of the present invention, since the third surface 5 is a totally reflecting surface and is not covered with reflective coating, the outside world light passing through the third surface 5 and the first surface 3 reaches the viewer's eye ball 15. Consequently, the outside world can be viewed in an area α different from the electronic image viewing area β . That the viewer can view the outside world image and the electronic image in different partial areas as mentioned above indicates, for example, that the viewer can simultaneously view the outside world in an upper area and the electronic image in a lower area in the viewer's field of view. The different partial areas may be areas arranged in any direction and parts such as upper and lower areas

or left and right areas as long as the viewer can view the two images in different partial areas, respectively.

By providing such a function, the viewer can recognize the outside world while wearing the image display apparatus, so that a safe image display apparatus can be provided that can prevent danger and deal with emergencies. As a result, the area of application as an image display apparatus is widened.

In the image forming apparatus, it is desirable that the image forming means be an image display device (one relayed by the relay optical system is not predetermined) such as a CLD, a CRT or the like of which image formed screen is disposed so as to be opposed to the fourth surface and the second surface be a curved surface.

Moreover, the image forming apparatus can be structured as a head-mounted image display apparatus by providing a holding member that holds the image display device and the eyepiece optical system before the viewer's eye ball, and forming the prism member so that the luminous flux emanating from the image display device is incident on the fourth surface, the incident luminous flux is reflected at the third surface, the reflected luminous flux is reflected at the first surface, the reflected luminous flux is reflected at the second surface and the reflected luminous flux exits from the first surface.

Moreover, in the image forming apparatus, it is desirable that the surface disposed immediately before the viewer's eye ball and the surface disposed on the outside world side of the eyepiece optical system be formed so that the composite optical power in given positions of the two surfaces is substantially zero with respect to the outside world light. When the composite optical power of the two surfaces with respect to the outside world light is substantially zero, the outside world image viewed through the image forming apparatus is substantially equal to the outside world viewed with the naked eye, so that a more natural outside world image can be viewed. Consequently, danger can be prevented and the outside world can precisely be recognized in an emergency, so that a very safe image display apparatus can be provided.

In this case, the first surface and the third surface may be curved surfaces, spherical

surfaces or plane surfaces. When the viewer views the outside world, the light ray from the outside world passes through the totally reflecting area of the internally reflecting surface disposed on the outside world side and the refracting surface disposed immediately before the viewer's eye ball to be projected onto the viewer's pupil. By the two surfaces being not aspherical but spherical, the curvatures of the surfaces do not change, so that viewing of a more natural off-axis outside world image is facilitated. Moreover, in a structure where the first surface disposed immediately before the viewer's eye ball and the third surface disposed on the outside world side of the eyepiece optical system are plane surfaces, since the surfaces have no optical power, a natural outside world image through a transparent plate, a very natural outside world image can be viewed.

Further, in a structure where the two surfaces are vertical to the viewer's axis of sighting and disposed so as to be parallel to each other, since the outside world is viewed merely through a transparent plate, a very natural outside world image can be viewed. In these structures, when the composite optical power with respect to the outside world light, in given positions of the surface disposed immediately before the viewer's eye ball and the surface disposed on the outside world side of the eyepiece optical system is ϕ_u , it is desirable that the following expression be satisfied:

$$-0.5 \leq \phi_u \leq 0.5 \text{ (1/mm)} \quad \dots (3)$$

Here, ϕ_u corresponds to each of the optical power $\phi_{u(yz)}$ within a plane including the axial principal ray and the optical power $\phi_{u(xz)}$ within a plane vertical to the surface including the axial principal ray. Since the magnification when the outside world light passes through the decentered prism can be set to a value close to 1 by satisfying the condition of the expression (3), a more natural outside world image can be viewed.

Moreover, in the image viewing apparatus, it is desirable that the prism member can be fixed in the same position both when an image formed by the image forming means is viewed and when the outside world image is viewed, and in that case, as described above with reference to FIG.

7. the image from the image forming means and the outside world image can be viewed in different partial areas through the first surface and the third surface.

The prism member may be provided with switching means for switching between viewing of an image formed by the image forming means and viewing of the outside world image, and be moved by the switching means.

That is, by moving the prism member so that the first surface of the eyepiece optical system disposed immediately before the viewer's eye ball and the third surface disposed on the outside world side and totally reflecting part of the principal ray are in the vicinity of the viewer's axis of sighting, the outside world image can be viewed in the periphery of the axis of sighting when the viewer faces straight forward, that is, in the vicinity of the center of the field of view, so that the viewer can recognize the outside world before his eyes while wearing the image display apparatus. Consequently, an image display apparatus ensuring safety can be realized.

Moreover, in a structure where the electronic image is kept displayed, by moving and returning the eyepiece optical system, the outside world image and the electronic image can be recognized while switching therbetween is made, so that the area of application is widened.

In this case, it is desirable that the surface disposed immediately before the viewer's eye ball and the surface disposed on the outside world side of the eyepiece optical system be formed so that the composite optical power of the two surfaces is substantially zero with respect to the outside world light. When the composite optical power of the two surfaces with respect to the outside world light is substantially zero, the viewer can view a more natural outside world image, so that danger can be prevented and emergencies can appropriately be dealt with. As a result, a very safe image display apparatus can be provided.

When the composite optical power, with respect to the outside world light, is given positions of the surface disposed immediately before the viewer's eye ball and the surface disposed on the outside world side of the eyepiece optical system is ϕ_a , it is desirable that the following

expression be satisfied:

$$-0.5 \leq \phi_a \leq 0.5 \text{ (1/mm)} \quad \dots (4)$$

Here, ϕ_a corresponds to each of the optical power $\phi_{\alpha(yz)}$ within a plane including the axial principal ray and the optical power $\phi_{\alpha(zx)}$ within a plane vertical to the surface including the axial principal ray. Since the magnification when the outside world light passes through the decentered prism can be set to a value close to 1 by satisfying the condition of the expression (4), a more natural outside world image can be viewed.

In this case, it is desirable for the switching means to move the prism member so that the optical path from the prism member to the viewer's eye ball when an image formed by the image forming means is viewed substantially coincides with the optical path from the prism member to the viewer's eye ball when the outside world image is viewed.

Moreover, in a structure where the prism member is moved in a direction along a plane including the optical path of the axial principal ray, since the prism member is linearly moved, the moving mechanism and the overall layout of the apparatus are simplified, so that an inexpensive image display apparatus can be realized.

Moreover, in a structure where the prism member is movable in a direction vertical to the axis of sighting, since not only the overall layout of the apparatus and the moving mechanism are simplified but also the amount of forward protrusion from the viewer is the same even after the eyepiece optical system is moved, a small size and compact image display apparatus can be provided.

Moreover, in a structure where the prism member is rotatable, since the outside world can be viewed by moving the prism member with a simple rotating mechanism, the mechanism itself is inexpensive, and further, in a structure where the prism members on the left and on the right can simultaneously be rotated, the outside world can be recognized with both eyes, so that safety increases and the layout of the apparatus can be realized with a simple structure.

In still another image viewing apparatus of the present invention having image forming means and an eyepiece optical system that directs an image formed by the image forming means to a viewing eye ball, the eyepiece optical system includes at least a prism member, the prism member has, in its surface structure, at least four optical property surfaces having an optical property of transmission or reflection, a space surrounded by the four optical property surfaces and a surface other than the four surfaces is filled with a single medium having a refractive index (n) higher than 1 ($n > 1$), the four optical property surfaces comprise: a first surface having a transmission property and a reflection property, and disposed on a side of a viewer's eye ball; a second surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be at least decentred or inclined with respect to the viewer's axis of sighting; a third surface having a reflection property and disposed so as to be opposed to the first surface with the medium in between and to be substantially adjacent to the second surface; and a fourth surface disposed so that one end thereof is substantially adjacent to the first surface and the other end thereof is substantially in the vicinity of the third surface, the prism member is structured so that at least the second surface or the third surface has a total reflection property and line of sight detecting means for detecting the viewer's line of sight is disposed in the vicinity of an area where total reflection by the second surface or the third surface having the total reflection property is caused. In this case, the surface other than the four optical property surfaces is also a prism side surface or a cut surface having no optical property.

Now, the action and effect when the image viewing apparatus is structured as an image display apparatus will be described. The disposition of the line of sight detecting means in the vicinity of the optical system enables detection of the viewer's line of sight. The detection of the line of sight will be described with reference to FIGS. 5 and 6. (a) of FIG. 5 is a cross-sectional view of an image display apparatus comprising a decentered prism 12 in which a space formed by three surfaces 3, 4 and 6 decentred with respect to the optical axis is filled with a medium having a refractive index higher than 1, and an image display device 7. FIG. 6 is a cross-sectional view of another image display apparatus comprising a decentered prism 12 in which a space formed by four surfaces 3, 4, 5 and 6 decentred with respect to the optical axis is filled with a medium having a refractive index higher than 1, and an image display device 7. In the figures, reference numeral 1 represents the viewer's pupil, reference numeral 2 represents the viewer's axis of sighting, reference numeral 3 represents a first surface of an eyepiece optical system 12, reference numeral 4 represents a second surface, reference numeral 5 represents a third surface, reference numeral 6 represents a fourth surface, reference numeral 7 represents the image display device, reference numeral 9 represents a line of sight detecting optical system, reference numeral 10 represents a line of sight detector, reference numeral 11 represents illuminating means, reference numeral 12 represents the eyepiece optical system, and the reference numeral 15 represents the viewer's eye ball.

(a) of FIG. 5 is a view in which the line of sight detecting means 9 and 10 are disposed on the outside world side opposed to the viewer's eye ball 15 with the decentered prism of the eyepiece optical system 12 in between. In this case, it is necessary for the image of the viewer's pupil 1 to pass through the first surface 3 disposed immediately before the viewer's pupil 1 and the second surface 4 which is a reflecting surface disposed on the outside world side of the eyepiece optical system 12, to be incident on the line of sight detecting means 9 and 10. However, since the second surface 4 disposed on the outside world side of the eyepiece optical system 12 is a reflecting surface covered with reflective coating to direct the image of the viewer's pupil 1 to the line of sight detecting means 9 and 10, it is necessary for the reflecting surface to have a part NC not covered with reflective coating (coating hole), which has a detrimental effect on the image being viewed.

(b) of FIG. 5 and FIG. 6 show image display apparatuses which are image viewing

refractive index higher than 1, and an image display device 7. (b) of FIG. 5 is a cross-sectional view of an image display apparatus comprising a decentered prism 12 in which a space formed by

apparatuses of the present invention. The third surface 5 which is a reflecting surface disposed on the outside world side of the eyepiece optical system 12 is set so that a part thereof totally reflects

light. It is unnecessary to cover the totally reflecting part with reflective coating because the totally reflecting part reflects light from the image display device 7 without covered with reflective coating and the image of the viewer's pupil 1 passes through the first surface 3 disposed immediately before the viewer's pupil 1 and the totally reflecting part of the third surface 5 disposed on the outside world

side of the eyepiece optical system, so that the image of the viewer's pupil 1 can be detected by the line of sight detecting means 9 and 10. Consequently, the line of sight can be detected without forming the coating hole that has a detrimental effect on viewing of the electronic image, in the reflecting surface of the eyepiece optical system.

In this case, it is desirable for the first surface of the decentered prism to have a total reflection property. In that case, it is desirable for the line of sight detecting means to be disposed in a position to detect the viewer's line of sight through the second surface or the totally reflecting area of the third surface.

Moreover, it is desirable to provide the illuminating means for illuminating the viewer's eye ball. In this image display apparatus, the viewer's line of sight can precisely be detected because a bright image can be detected by illuminating the viewer's eye ball. Moreover, it is desirable that the illuminating means be disposed on the outside world side of the eyepiece optical system. When the illuminating means 11 is disposed between the viewer's face and the eyepiece optical system 12 like (a) of FIG. 5, there is a possibility that it interfaces with glasses or the like. However, by disposing the illuminating means 11 on the outside world side of the eyepiece optical system 12 like (b) of FIG. 5, the interference with the viewer's face can be avoided. Further, by disposing the illuminating means 11 so that the illuminating light from the illuminating means 11 passes through the totally reflecting part of the reflecting surface of the eyepiece optical system 12, the viewer's pupil can be illuminated without the coating hole formed. Moreover, it is desirable for

the illuminating means to use infrared light. That an electronic image is viewed indicates that the viewer's pupil is illuminated by light of the image display device. In the line of sight detecting means required to capture a feasible virtual image and perform image analysis such as one employing a corneal reflex method, it is necessary to eliminate the reflection image caused by the luminous flux of the image display device of which light emanation amount changes from moment to moment. Normally, the image display device is an LCD or the like, and the emanating light is in a waveband of the visible region. Therefore, the influence of light from the image display device can be reduced by the illuminating means using infrared light.

In this case, the image viewing apparatus can also be structured as a head-mounted image display apparatus by providing a holding member that holds the eyepiece optical system, the image forming means and the line of sight detecting means before the viewer's face.

Moreover, the image forming apparatus can be provided with positioning means for positioning the image forming means and the eyepiece optical system with respect to the viewer's head.

Further, it can be made possible to view a three-dimensional image or the like with both eyes by providing supporting means for supporting at least two pairs of such image forming apparatuses with a predetermined interval in between.

Next, in an image display apparatus according to the present invention having an image display device and an eyepiece optical system that directs an image formed by the image display device so that it can be viewed as a virtual image, the eyepiece optical system includes: a decentered prism in which a space formed by at least two surfaces is filled with a medium having a refractive index higher than 1 and at least one of a first surface situated immediately before the viewer's eye ball and a second surface which is a reflecting surface opposed to the first surface is a curved surface decentered or inclined with respect to the viewer's axis of sighting; and aberration correcting means disposed outside the second surface and for correcting aberrations caused with respect to the outside

world light on the first surface and the second surface by decentring.

In the image display apparatus, when the outside world image is viewed through the first surface situated immediately before the viewer's eye ball and the second surface which is a reflecting surface opposed to the first surface, since at least one of the two surfaces is decentered or inclined with respect to the viewer's axis of sighting, the viewed outside world image is similar to one viewed through a lens having an optical power biased asymmetrically with respect to the optical axis. Therefore, by disposing aberration correcting means such as a Fresnel lens that cancels the optical power of the second surface biased toward the outside world side, the viewer can view a more natural outside world image. Further, since the Fresnel lens is a very thin optical element, a small-size image display apparatus can be provided without the size increased.

Moreover, in the present invention, the Fresnel lens may be replaced by a different optical element such as a diffraction optical element or a holographic optical element as long as the above-mentioned effect is obtained.

When a Fresnel lens is used, it is desirable that the center of the zone of the Fresnel lens be situated within a plane including the optical path of the axial principal ray from the image display device and the Fresnel lens be decentered vertically to the axis of sighting within the plane including the optical path of the axial principal ray. The use of a Fresnel lens having an axially symmetrical configuration which is excellent in manufactureability enables cost reduction. By disposing a Fresnel lens having an axially symmetrical optical power so as to be decentered with respect to the axis of sighting within the plane including the optical path of the axial principal ray, aberration is caused with respect to the outside world light on the first surface and the second surface by decentring can more excellently be corrected.

Moreover, the Fresnel lens may be disposed in a manner such that the center of the zone of the Fresnel lens is situated on the plane including the optical path of the axial principal ray, that the Fresnel lens is inclined with respect to the axis of sighting and that the direction of the inclination is

along the configuration of the second surface. Disposing the Fresnel lens along the configuration

of the second surface is disposing it so as to be inclined with respect to the viewer's axis of sighting. Therefore, the optical power can be set to a biased optical power being asymmetric with respect to the optical axis, so that aberrations caused with respect to the outside world light on the first surface and the second surface by decentring can more excellently be corrected. Further, the amount of protrusion with respect to the viewer and the space between the eyepiece optical system and the Fresnel lens are reduced, so that a very compact image display apparatus without an unnecessary space can be provided.

In another image forming apparatus of the present invention having an image display device and an eyepiece optical system that directs an image formed by the image display device so that it can be viewed as a virtual image, the eyepiece optical system includes: a decentered prism in which a space formed by at least three surfaces is filled with a medium having a refractive index higher than 1, the at least three surfaces comprise a refracting and internally reflecting surface situated immediately before the viewer's eye ball; an outside world side internally reflecting surface disposed on the outside world side of the eyepiece optical system so as to be opposed to the refracting and internally reflecting surface, and a reflecting surface on which the luminous flux emanating from the image display device is incident, at least one of the surfaces is decentered or inclined with respect to the viewer's axis of sighting, and internal reflection occurs at least three times; and a second optical element that cancels the optical power caused with respect to the outside world light on the second surface when the outside world is viewed through the refracting and internally reflecting surface situated immediately before the viewer's eye ball and the outside world side reflecting surface, and the second optical element is disposed on the outside world side of the outside world side internally reflecting surface.

When the outside world image is viewed through the first surface situated immediately before the viewer's eye ball and the second surface which is a reflecting surface opposed to the first

surface, since at least one of the two surfaces is decentered or inclined with respect to the viewer's axis of sighting, the viewed outside world image is similar to one viewed through a lens having a biased optical power that varies according to the image height. Therefore, by disposing the second optical element that cancels the biased optical power caused with respect to the outside world light on the second surface, on the outside world side of the eyepiece optical system, the viewer can view a more natural and wider-area outside world image. Consequently, a safe image display apparatus can be provided that can prevent danger and deal with emergencies.

In this case, the eyepiece optical system may comprise a decentered prism in which a space formed by four surfaces is filled with a medium having a refractive index higher than 1, the four surfaces comprise a first surface which is a refracting and reflecting surface situated on the side of the viewer's eye ball, a second surface which is a reflecting surface opposed to the first surface, a third surface which is a reflecting surface opposed to the first surface and adjoining the second surface, and a fourth surface which is a refracting surface closest to the image display device, and at least one of the surfaces is decentered or inclined with respect to the viewer's axis of sighting. When the eyepiece optical system comprises four surfaces as described above, the outside world is recognized by the outside world light having passed through the first surface and the second surface. In that case, by disposing a second optical element that cancels the biased optical power only in an area covered by the second surface, an additional function can be realized without the overall size of the eyepiece optical system increased.

Moreover, it is desirable to dispose at least one second optical element on the outside world side of the second surface or the third surface so that the outside world can be viewed through the first surface, the second surface and the second optical element, or the first surface, the third surface and the second optical element. By disposing the second optical element that cancels the biased optical power on the outside world side of the second surface, a natural outside world image can be viewed in an area substantially the same as the area in which the electronic image is viewed.

Likewise, by disposing the second optical element that cancels the biased optical power on the outside world side of the third surface, a natural outside world image can also be viewed in an area different from the area in which the electronic image is viewed. By disposing two second optical elements one on the outside world side of the second surface and the other on the outside world side of the third surface, the viewer can view all the outside world images that pass through the first and the second surfaces and the first and the third surfaces. Consequently, the outside world viewing angle is wider than the electronic image viewing angle, so that a natural and wide-area outside world image can be viewed. As a result, a very safe image display apparatus can be provided that can prevent danger and appropriately deal with emergencies.

Moreover, it is desirable for the second optical element to simultaneously cancel the composite optical power of the first and the second surfaces or the first and the third surfaces with respect to the outside world light. By forming the second optical element that simultaneously cancels the composite optical powers of the first and the second surfaces and the first and the third surfaces with respect to the outside world light, of one optical element, and disposing it on the outside world side of the eyepiece optical system, a wide area of outside world can be viewed. Since this second optical element simultaneously cancels the composite optical powers, there is no gap in the outside world image, so that a more natural outside world image can be viewed. Consequently, a wide area of outside world can be recognized with one optical element, so that a low-cost and safer image display apparatus can be provided that can prevent danger and deal with emergencies.

Moreover, in the above-described structure, positioning means can be provided for positioning the image display device and the eyepiece optical system with respect to the viewer's head. By providing the positioning means for positioning the image display device and the eyepiece optical system with respect to the viewer's head, the viewer can view a stable electronic image.

Moreover, the image display apparatus can be mounted on the viewer's head by providing supporting means for supporting the image display device and the eyepiece optical system with respect to the viewer's head. By providing the supporting means for supporting the image display device and the eyepiece optical system with respect to the viewer's head so that the image display apparatus can be mounted on the viewer's head, the viewer can view the electronic image in whatever viewing positions and viewing directions he likes.

Further, supporting means for supporting at least two pairs of image display apparatuses with a predetermined interval in between can be provided. By providing the supporting means for supporting at least two pairs with a predetermined interval in between, the viewer can easily view images with the left and the right eyes. Moreover, by displaying images where a parallax is provided between the left and the right electronic images and viewing them with both eyes, a three-dimensional image can be enjoyed.

Moreover, the eyepiece optical system in the above-described image display apparatus can be used as an imaging optical system. The eyepiece optical system can be used as an imaging optical system such as a finder optical system of a camera as shown in FIG. 24 by forming it so as to image an object at infinity with the image display surface thereof as an image surface.

In the present invention, one surface may be used both as the second surface and the third surface. In that case, since the physical number of surfaces can be reduced by one, the process can be simplified in optical design and in prism manufacture, which contributes to mass productivity and price reduction. Further, by using physically one surface having both the property of the second surface and the property of the third surface as the second and the third surfaces and setting the areas in which the luminous flux is internally reflected so as to overlap each other, size reduction of the prism member can be realized.

[Embodiments of the Invention] Hereinafter, first to seventeenth embodiments of the image display apparatus according to the present invention will be described. In the structural

parameters of the embodiments described below, as typically shown in FIG. 1, an exit pupil 1 of an

eyepiece optical system 12 is the origin of the optical system; an optical axis 2 is defined by a light ray passing through the center of display of an image display device 7 and the center (origin) of the exit pupil 1, the direction in which the optical axis 2 extends from the exit pupil 1 is the z-axis direction, the direction that is perpendicular to the z-axis, passes through the center of the exit pupil 1 and is within a plane where the light ray is bent by the eyepiece optical system 12 is the y-axis direction, a direction that is perpendicular to the z-axis and the y-axis and passes through the center of the exit pupil 1 is the x-axis direction, a direction from the exit pupil 1 to the eyepiece optical system 12 is the positive z-axis direction, a direction from the optical axis 2 to the image display device 7 is the positive y-axis direction, and a direction constituting a right-hand system together with the z-axis and the y-axis is the positive x-axis direction. Ray tracing is performed according to backward ray tracing with the exit pupil 1 side of the eyepiece optical system 12 as the object side and the image display device 7 side thereof as the image side.

With respect to the surfaces for which decentring amounts Y and X and an inclination amount θ are provided, the decentring amounts Y and X and the inclination amount θ represent the amounts of shift in the y direction and the z direction from the exit pupil 1 which is the origin of the optical system and the angle of inclination of the central axis of the surface with respect to the z-axis unless otherwise specified in the structural parameters (there is specification in the sixth and the ninth embodiments). The angle of inclination is positive counterclockwise. When a reference surface is specified, the decentring amounts Y and X and the inclination amount θ represent similar shift amounts and inclination angle from the vertex of the reference surface.

In the structural parameters shown below, axial distances in coaxial parts are shown as distances. In addition, the radii of curvature of the spherical surfaces, the refractive indices of the media and the Abbe numbers are shown according to the conventional method.

FIGs. 1 to 4, (b) of FIG. 5 and FIGs. 6 to 17 are cross-sectional views of image display

apparatuses of the first to the fourth, the fifth and the sixteenth to the seventeenth embodiments of the present invention including the optical axis. The embodiments of FIGs. 1 to 4, (b) of FIG 5,

FIGs. 6 to 11 and FIGs. 15 and 16 comprise a decentered prism 12 in which a space formed by four surfaces 3, 4, 5 and 6 decentered with respect to the optical axis is filled with a medium having a refractive index higher than 1, and the embodiment of FIG. 17 comprises a decentered prism 12 in which a space formed by three surfaces 3, 4 and 6 decentered with respect to the optical axis is filled

with a medium having a refractive index higher than 1. In the figures, reference numeral 1 represents the viewer's pupil, reference numeral 2 represents the viewer's axis of sighting, reference numeral 3 represents a first surface of an eyepiece optical system 12, reference numeral 4 represents a second surface, reference numeral 5 represents a third surface, reference numeral 6 represents a fourth surface, reference numeral 7 represents an image display device, reference numeral 8 represents a Fresnel lens, reference numeral 9 represents a line of sight detecting optical system.

reference numeral 10 represents a line of sight detector, reference numeral 11 represents illuminating means, reference numeral 12 represents the eyepiece optical system (decentered prism), reference numerals 13 and 14 represent second optical elements, reference numeral 15 represents the viewer's eye ball, reference numeral 16 represents an optical filter, reference numeral 17 represents a linear motor, reference numeral 18 represents protrusions provided on an optical element, and reference numeral 19 represents a guide (rail) provided on an exterior portion. With respect to the actual light ray path when an electronic image is viewed, in the embodiments of FIGs. 1 to 4, (b) of FIG 5, FIGs. 6 to 11 and FIGs. 15 and 16, the light ray emanating from the electronic image on the image display device 7 is incident on the fourth surface 6 which is a refracting surface opposed to the image display device 7 of the eyepiece optical system 12, is reflected at, of the two surfaces 4 and 5 situated opposite to the viewer's face, the third surface 5 adjoining the fourth surface 6 toward the side of the viewer's pupil 1, is reflected at the first surface 3 disposed immediately before the viewer's pupil 1 in a direction for the light ray to retrace from the viewer's pupil 1, is reflected at, of

the two surfaces 4 and 5 situated opposite to the viewer's face, the second surface 4 disposed immediately before the viewer's pupil 1 toward the side of the viewer's pupil 1, and passes through

the first surface 3 to be projected within the viewer's eye ball 15 with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1. In the embodiment of FIG. 17, the light ray emanating from the electronic image on the image display device 7 is incident on the fourth surface 6 which is a refacting surface opposed to the image display device 7 of the eyepiece optical

system 12, is reflected toward the side of the viewer's pupil 1 at an area (the third surface 5), adjoining the fourth surface 6, of the second surface 4 situated opposite to the viewer's face and used also as the third surface 5, is reflected at the first surface 3 disposed immediately before the viewer's pupil 1 in a direction for the light ray to retrace from the viewer's pupil 1, is reflected toward the side of the viewer's pupil 1 at an area of the second surface 4 which area is situated opposite to the viewer's face and far from the fourth surface 6, and passes through the first surface 3 to be projected within the viewer's eye ball 15 with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1.

The ones shown in (b) of FIG. 5 and FIG. 6 are embodiments of the image display apparatus of the present invention having the line of sight detecting means. The third surface 5 which is a reflecting surface disposed on the outside world side of the eyepiece optical system 12 is set so that a part thereof totally reflects light. It is unnecessary to cover the totally reflecting part with reflective coating because the totally reflecting part reflects light from the image display device 7 without covered with reflective coating. The actual light ray path when the line of sight is detected is such that the illuminating light from the light source 11 passes through the third surface 5 and the first surface 3 of the eyepiece optical system 12 to illuminate the viewer's eye ball 15 and the light ray reflected thereat is incident on the first surface 3 disposed immediately before the viewer's pupil 1, passes through the totally reflecting area which is at least a part of the third surface 5 situated opposite to the viewer's face, and is directed to the line of sight detector 10 by the line of

sight detecting optical system 9 to form an image of the viewer's pupil 1. Needless to say, the illuminating means 11 using infrared light and the detector 10 detecting infrared light may be used to reduce the influence of light on the electronic image and the like. Further, the illuminating means 11 may be disposed in a position other than the shown position or in any position as long as the viewer's eye ball 15 can be illuminated.

FIG. 18 is a cross-sectional view of an embodiment in which similar line of sight detecting means comprising the line of sight detecting optical system 9, the line of sight detector 10 and the light source 11 is provided in the case of the eyepiece optical system 12 comprising the three surfaces 3, 4 and 6 decentered with respect to the optical axis like the seventeenth embodiment. The actual light ray path when the line of sight is detected will not be described because it is similar to that of (b) of FIG. 5 and FIG. 6.

The one shown in FIG. 7 is an embodiment of the image display apparatus of the present invention with which the electronic image and the outside world image can simultaneously be viewed through the eyepiece optical system 12. The actual light ray path when the outside world image is viewed is such that the light ray from the object point of the outside world passes through the first surface 3 and is projected within the viewer's eye ball with third surface 5, passes through the first surface 3 and is projected within the viewer's eye ball with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1. Further, by disposing on the outside world side of the third surface 5 an attenuating filter or the optical element 16 that adjusts the quantity of the outside world light, the viewer can easily view both of the electronic image and the outside world image. Moreover, by making the attenuating filter or the optical element 16 movable between the viewing areas α and β , the light quantity of either the electronic image or the outside world image can be controlled.

The ones shown in FIGs. 8 and 9 are embodiments of another image display apparatus of the present invention with which the outside world image can be viewed by moving the eyepiece optical system 12. In FIG. 8, the eyepiece optical system 12 is shifted to the outside world image

viewing position of (b) of FIG. 8 by moving it from the electronic image viewing position of (a) of FIG. 8 in the negative Y direction with respect to the viewer's pupil. In FIG. 9, the eyepiece optical system 12 is shifted to the outside image viewing position of (b) of FIG. 9 by rotating it clockwise from the electronic image viewing position of (a) of FIG. 9 with respect to the viewer's pupil 1. Consequently, in either case, the outside world can be viewed through the eyepiece optical system 12 in the direction of the viewer's axis of sighting. The light ray from the object point of the outside world is incident on the third surface 5 and passes through the first surface 3 to be projected within the viewer's eye ball with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1. Further, in (b) of FIG. 8, the viewer can view the electronic image in an area below the viewer's axis of sighting 2. The electronic image viewing direction may be any direction because it varies according to the manner of disposition or the direction of movement of the eyepiece optical system 12.

(c) of FIG. 8 and (c) of FIG. 9 each show an example of a mechanism for moving the eyepiece optical system 12. In either case, the eyepiece optical system 12 is moved along the guide (rail) 19 provided on the exterior portion by the linear motor 17 through the protrus ions 18 provided on the optical element. In the case of (c) of FIG. 8, the guide (rail) 19 is linear, whereas in the case of (c) of FIG. 9 the guide (rail) 19 is arc-shaped, so that the eyepiece optical system 12 is linearly moved and rotated in these cases, respectively.

FIG. 19 shows an example in which in the case of the eyepiece optical system 12 comprising the three surfaces 3, 4 and 6 decentered with respect to the optical axis like the seventeenth embodiment, the eyepiece optical system 12 is shifted to the outside world image viewing position by moving it from the electronic image viewing position in the negative Y direction with respect to the viewer's pupil like the embodiment of FIG. 8. The action thereof will not be described because it is similar to that of FIG. 8.

The ones shown in FIGs. 10 to 14 are embodiments of the image display apparatus of the

present invention in which the Fresnel lens 8 which is the aberration correcting means is disposed on

the optical path when the outside world image is viewed. The actual light ray path when the outside world image is viewed is such that the light ray from the object point of the outside world passes through the Fresnel lens 8 to be incident on the second surface 4 of the decentered prism and passes through the first surface 3 to be projected within the viewer's eye ball with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1. It is necessary to situate the Fresnel lens 8 in a predetermined position only when the outside world is viewed. When the

mechanism that vertically moves or rotates the Fresnel lens 8, or the Fresnel lens 8 may be rotated around its vertical axis.

Of FIGs. 10 to 14, in the cases of FIGs. 10 and 11, like FIG. 1 and the like, the eyepiece optical system (decentered prism) 12 comprises the four surfaces 3, 4, 5 and 6 decentered with respect to the optical axis and the light ray path when the electronic image is viewed is similar.

While the translation from 12 to FIG. 12 comprises the decentered prism 12 in which a space

However, the eccentricity of the electron beam is increased when the electron gun is tilted, as shown in Fig. 1. The beam is formed by the three surfaces 3, 4 and 6 decentred with respect to the optical axis when the electron gun is tilted.

image is viewed is such that the light ray emanating from the electronic image on the image display

device 7 is incident on the fourth surface (being third in the order of surfaces) 6 which is a refracting surface opposed to the image display device 7 of the eyepiece optical system 12, is reflected at the first surface 3 disposed immediately before the viewer's pupil 1 in a direction for the light ray to recede from the viewer's pupil 1, is reflected at the second surface 4 situated opposite to the viewer's

face toward the side of the viewer's pupil 1, and passes through the first surface 2000 to project within the viewer's eye ball 15 with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1.

Moreover, the decentered prism 12 of FIG. 13 comprises the decentered prism 12 in which

a space formed by the three surfaces 3, 4 and 6 decentred with respect to the optical axis is filled

with a medium having a refractive index higher than 1, and the actual light ray path when the electronic image is viewed is such that the light ray emanating from the electronic image on the image display device 7 is incident on the fourth surface (being third in the order of surfaces) 6 which is a refracting surface opposed to the image display device 7 of the eyepiece optical system 12, is reflected at the second surface 4 situated opposite to the viewer's face toward the side of the viewer's pupil 1, and passes through the first surface 3 to be projected within the viewer's eye ball 15 with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil 1.

Moreover, the decentered prism 12 of FIG. 14 comprises the decentered prism 12 in which a space formed by the two surfaces 3 and 4 decentered with respect to the optical axis is filled with a medium having a refractive index higher than 1, and the actual light ray path when the electron image is viewed is such that the light ray emanating from the electronic image on the image display device 7 is incident on the first surface 3 which is a refraacting surface opposed to the image display device 7 of the eyepiece optical system 12, is reflected at the second surface 4 situated opposite to the viewer's face toward the side of the viewer's pupil 1, and passes through the first surface 3 to be projected within the viewer's eye ball 15 with the position of the viewer's iris or the center of the eye ball as the exit pupil 1.

Next, the ones shown in FIGS. 15 and 16 are embodiments of the image display apparatus of the present invention in which the second optical elements 13 and 14 that cancel the optical power caused on the two surfaces 3 and 4 or 3 and 5 with respect to the outside world light when the outside world is viewed through the first surface 3 of the eyepiece optical system 12 situated immediately before the viewer's eye ball and the second surface 4 or the third surface 5 which is an outside world side internally reflecting surface are disposed on the optical path when the outside world is viewed. The actual light ray path when the outside world image is viewed is such that the light ray from the object point of the outside world passes through the second optical element 13 or

the other second optical element 14 to be incident on the second surface 4 or the third surface 5 of the decentered prism 12, and passes through the first surface 3 to be projected within the viewer's eye ball with the position of the viewer's iris or the center of rotation of the eye ball as the exit pupil.

1.

A monocular image display apparatus may be structured by providing one pair of eyepiece optical system and image display device as described above, or a binocular image display apparatus may be structured by providing such a pair on each of the left and the right and holding them in positions spaced the interpupillary distance apart. By doing so, the present invention can be structured as a fixed or a portable image display apparatus with which images can be viewed with one eye or both eyes.

A case of the monocular image display apparatus is shown in FIG. 21 (in this case, mounted on the left eye), and a case of the binocular image display apparatus is shown in FIG. 22. In FIGs. 21 and 22, reference numeral 31 represents the main unit of the image display apparatus which is fixed by a supporting member through the head so as to be held before the left eye on the viewer's face in the case of FIG. 21 and before both eyes on the viewer's face in the case of FIG. 22.

The supporting member comprises left and right front frames 32 having one ends joined to the main unit 31 and extending from the viewer's temples to above the viewer's ears, and left and right rear frames 33 joined to the other ends of the front frames 32 and extending along side parts of the viewer's head (in the case of FIG. 21), or comprises, in addition to the front and the rear frames 32 and 33, a vertex frame 34 having its ends joined to the other ends of the left and right rear frames 33, respectively, so as to be sandwiched therebetween, and supporting the vertex part of the viewer's head (in the case of FIG. 22).

Moreover, in the vicinity of the joints of the front frames 32 to the rear frames 33, rear plates 35 comprising an elastic body such as a metal plate spring are joined. The rear plates 35 are each joined so that a rear cover 36 constituting a part of the supporting member is situated in the rear of the viewer's ear in a part ranging from the back of the head to the base of the neck so as to be supportable (in the case of FIG. 22). A speaker 39 is attached in a position corresponding to each of the viewer's ears within the rear plate 35 or the rear cover 36.

A cable 41 for externally transmitting signals such as video and sound signals passes from

the main unit 31 through the vertex frame 34 (in the case of FIG. 22), the rear frame 33, the front frame 32 and the rear plate 35 to outwardly protrude from the rear end of the rear plate 35 or the rear cover 36.

The cable 41 is connected to a video reproducing apparatus 40. In the figure, reference numeral 40a represents a switch and a volume controller of the video reproducing apparatus 40.

An end of the cable 14 may be a jack so that the cable 41 is attachable to an existing video deck or the like. Further, the cable 41 may be connected to a TV tuner to realize an image display apparatus for TV watching, or may be connected to a computer so that computer graphics images or message images from the computer are received. Moreover, to exclude the obstructive code, an antenna may be connected so that external signals are received by radio waves.

When used as an imaging optical system, the eyepiece optical system of the image display apparatus of the present invention can be used, for example, as a finder optical system F1 of a compact camera Ca as shown in FIG. 23 in which a taking optical system Ob and the finder optical system F1 are separately provided. The structure of a n optical system when the eyepiece optical system is used as an imaging optical system is shown in FIG. 24. An objective optical system L1 can be formed of a front lens unit GF, an aperture diaphragm D and the eyepiece optical system DS of the present invention disposed in the rear thereof. The image formed by the objective optical system L1 is erect by a four -reflection Porro prism P provided on the viewer side of the objective optical system L1, and viewed through an eyepiece lens Oc.